LUVOIR ARCHITECTURE "A" ENGINEERING STATUS

Presented to: The LUVOIR STDT

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We will study two architectures in depth...

• Architecture A (first half of 2017)

- 15-m diameter aperture
- Five instrument bays:
 - Optical / NIR Coronagraph (A)
 - UV Multi-object Spectrograph ("LUMOS")
 - High-definition Imager (will also perform guiding / wavefront sensing)
 - UV Spectro-polarimeter (CNES Contributed)
 - Empty Bay for future expansion / contribution

Architecture B (late 2017 into 2018)

- ~9-m diameter aperture
- Three instrument bays:
 - Optical / NIR Coronagraph (B)
 - UV Multi-object Spectrograph ("LUMOS")
 - Optical / NIR Multi-resolution Spectrograph
 - Will need to include guiding and wavefront sensing capabilities

Study Schedule (2017):

- √ 1/17–24 Telescope Instrument Design Lab (IDL)
 - Pre-work 1/10
- √ 2/6–10 HDI IDL
 - Pre-work 1/31
- 3/20–24 Coronagraph IDL
 - Pre-work 3/14
- 5/15–19 LUMOS IDL
 - Pre-work 5/9
- 6/7–13 Instrument Accommodation & ΔTelescope IDL
 - Pre-work 6/1
- 7/10–14 LUVOIR "A" Mission Design Lab (MDL)
- June Dec.: Prepare Interim Report on Architecture A
- Sept.: Kick-off Architecture B IDLs

Telescope Design

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LUVOIR "A" Science Measurement Concept

- FOV: 10 arcmin x 8 arcmin
- Wavelength:
 - 100 nm 2.5+ μm
 - 90 nm blue cutoff stretch goal (largely dependent on coating technology development)
 - Optics & coatings should not preclude observations as red as 5.0 μm
- Diffraction-limited at 500 nm
- Spatial resolution:
 - Limiting instrument (LUMOS) has a spatial resolution of 30 mas for an assumed 25 μ m resolution element
 - Implies a telescope focal length \geq 172 m
- Aperture diameter:
 - Largest that can fit in an 8.4-meter x 27.4-meter fairing
 - Deemed to be 15-m by LUVOIR Engineering Team
- Operating temperature: 270 K

LUVOIR "A" Telescope Optical Design



LUVOIR "A" Telescope Aperture



- 1.15-m flat-to-flat segments (120x)
 - Central ring of array removed to accommodate Aft-optics & Secondary Mirror Obscuration
- Effective area is ~135 m^2
- 15-m circumscribed diameter / 12.7-m inscribed diameter
- Assumes 6 mm gaps



Mechanical Design Details (1)



Mechanical Design Details (2)



Stowed Telescoping Boom is 1.5 m deep

Mechanical Design Details (3)

Secondary Mirror





Footprint for Backplane Support Frame (BSF) and Instruments, given OTE stowed arrangement

Mechanical Design Details (4)

Not Shown:

6' tall

Fairing

Guard

- Sunshield and deployment system
- Spacecraft bus
- Primary Mirror "frill"







Mechanical Design Details (5)



Control System Block Diagram (So Far)



Concept for PM Segment Phasing (1)

- Introduced a closed-loop control system at the primary mirror segments to maintain segment-tosegment phasing
- Edge sensors on each segment measure picometer-level rigid-body motions at high speeds
- In response, piezoelectric (PZT) actuators move PM segments at picometer level
- Closed-loop system creates a "virtual monolith"

Concept for PM Segment Phasing (2) Edge Sensors

- Capacitive edge sensors
 - Two sensors per edge shared between segments: 622 sensors total
 - Provide 6-degree of freedom motion of each segment
- Similar sensors are being developed for ground-based systems (TMT, EELT, GMT) and have been used on Keck
- Challenge for LUVOIR is in the electronics
 - Need high speed (~450 Hz) readout with picometer-level accuracy at low power
- Lab-based system has demonstrated ~10 pm sensing at lower speeds with custom electronics

Concept for PM Segment Phasing (3) Segment Actuators

- Average the 450 Hz edge sensor measurements at a rate of 5:1 to generate a 90 Hz control signal for PM segments
- LUVOIR PM segments use exact same actuator design as JWST, except fine stage mechanical actuator is replaced with a PZT actuator
 - One PZT per actuator → 6 PZTs per PM segment for fine control of six degrees of freedom
- On JWST, a mechanical linkage is used to "step-down" physical actuator displacement to PM segment motion
 - i.e. if actuator moves 100 microns, the mirror only moves ~1 micron
- We will use the same linkage for the PZTs such that a 0.250 nm PZT step (which is easy) corresponds to ~2 pm motion of the mirror segment

Priority Telescope "To-Do"

- Add mechanical design fidelity to:
 - Primary mirror backplane
 - Primary mirror segment mechanical structure (heater, whiffles, delta frame, actuators, mounting points)
- Perform dynamic stability analysis
 - For launch loads on stowed configuration
 - For jitter disturbance on deployed configuration
- Re-visit thermal control system
 - Incorporating new backplane wing sections
 - Incorporating actuator drive electronics in each primary mirror segment assembly
- Add fidelity to mechanisms
 - Launch locks, deployment motors, latches, snubbers, etc.
- Perform straylight analysis and size baffling

High Definition Imager Design

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HDI Technical Overview (1/2)

- Two-channel Imaging Instrument:
 - UV/Vis Imaging (200 nm ~1.0 μm)
 - Diffraction-limited performance at 500 nm
 - Nyquist sampled at 400 nm
 - NIR Imaging (~1.0 μm 2.5 μm)
 - $\circ~$ Diffraction-limited performance at 1.2 μm
 - $\circ~$ Nyquist sampled at 1.2 μm
- Each channel will contain a suite of spectral filters:
 - Narrow (R ~50-100)
 - Medium (R ~20-40)
 - Broadband (R ~3-5)
 - At least one slitless grism/prism option with R ~200-500
- Field-of-view: 2 x 3 arcmin
 - Both channels view the same patch of sky

HDI Technical Overview (2/2)

• Exposure times:

- For most extragalactic sources and stellar population observations:
 - Total observation times of up to 200 hrs.
 - Composed of many exposures of 500-1000 s each
- High-speed photometry will require exposures of 50 100 ms
 - Will only be required over a small area of the focal plane array (perhaps a single SCA of the entire FPA)

• Dynamic Range:

 Desire the ability to define a region of the focal plane with reduced sensitivity (or faster readout) for both astrometry and solar system observations

HDI Special Modes :

- High-Precision Astrometry (for measuring exoplanet mass)
 - Astrometric precision of $< 5 \times 10^{-4}$ pixels
 - Requires a Pixel Calibration System to calibrate pixel geometry
- Fine-guiding
 - HDI is the primary fine-guidance sensor for the LUVOIR observatory
 - Similar to WFIRST operation
 - Requires ability to define regions of focal plane with faster readout
 - Should have capability in both UV/Vis and NIR channels
- Image-based Wavefront Sensing (i.e. phase retrieval) for telescope commissioning and maintenance
 - Similar to role played by NIRCam on JWST
 - Requires inclusion of:
 - Weak-lenses for generating defocused images
 - Dispersed Hartmann Sensor (DHS) gratings for coarse piston sensing
 - Pupil Imaging Lens (PIL) subsystem

HDI Detector Concept – UV/Vis Channel

CMOS Detector \bigcirc

- Pixel size = $5 \mu m$
- Nyquist sampled at 400 nm
 - Defined as: 1 pixel = λ / (2*D)
 - $\lambda = 400 \text{ nm}; D = 15.08 \text{ m}; 0 \text{ m}; 1 \text{ pixel} = 2.74 \text{ mas}$
- Read noise: ~2.5 e- \bullet
- Dark Current: Assume 0.001 e-/pix/s lacksquare
- Assume same QE as WFC3 UVIS CCD detector
- Operating temperature ~120 K \bullet



- Use 5 x 8 tiling of arrays: ۲

 - 40,960 x 65,536 pixels = 2.68 Gpix
- Gaps are as shown at right:
- Assume 16 bits/pixel: 5.4 Gbytes per image \bigcirc



HDI Detector Concept – NIR Channel

- H4RG Detector
 - Pixel size = 10 μm
 - Nyquist sampled at 1200 nm
 - Defined as: 1 pixel = λ / (2*D)
 - \circ λ = 1200 nm; D = 15.08 m; \Diamond 1 pixel = 8.2 mas
 - Read noise, dark current, QE adopted from WFIRST H4RG specs
 - Operating temperature ~70 K





HDI Thermal Design

 Three thermal zones within the instrument using passive cooling:

• 260 K

- Instrument housing
- Pupil relay optics
- UVIS channel optics
- 120 K
 - NIR channel optics
 - UVIS focal plane
- 70 K
 - NIR focal plane

Priority HDI "To-Do"

- Resolve a small volume allocation violation
 - A few millimeters of the NIR channel thermal shroud encroaches beyond the allocated instrument volume
- Finalize optical design
 - Grisms, weak lenses, pupil imaging lens, etc.
 - Investigate optimizing the design for UVIS throughput
- Re-visit thermal design and radiator sizing for the three thermal zones
 - 120 K may be colder than is needed for UVIS detector
- Re-visit number of elements and element type in the channel select mechanism