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# **LUV O I R – Lockheed Martin Cooperative Agreement Progress Report**

**Larry Dewell, Alison Nordt  
Lockheed Martin Space, Advanced Technology Center  
Palo Alto, California**

**Key Contributors:  
Kiarash Tajdaran, Shawn Wood**

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# Cooperative Agreement Technical Objectives



- **Task 1: System-level architecture and performance predication of a non-contact vibration isolation system**
  - Assessment of architecture support for observatory line-of-sight agility requirements
  - Integrated control/structure/optics modeling of a reference LUV O I R architecture with a non-contact interface, and frequency-domain prediction of LOS stability performance in the presence of spacecraft disturbances
  - Documents and engineering details to support non-contact isolation system integration into architecture baseline (Master Equipment List, system-level block diagrams, performance models, contribution to Conops)
- **Task 2: Instrument-Level AI&T Planning support**
  - Develop I&T plans and schedules for the LUV O I R Instruments:
    - Extreme Coronagraph for Living Planetary Systems (ECLIPS)
    - LUV O I R Ultraviolet Multi-Object Spectrograph (LUMOS)
  - Outline instrument-level activities up to delivery to “OTIS” integration
    - OTIS = Optical Telescope Element + Instruments

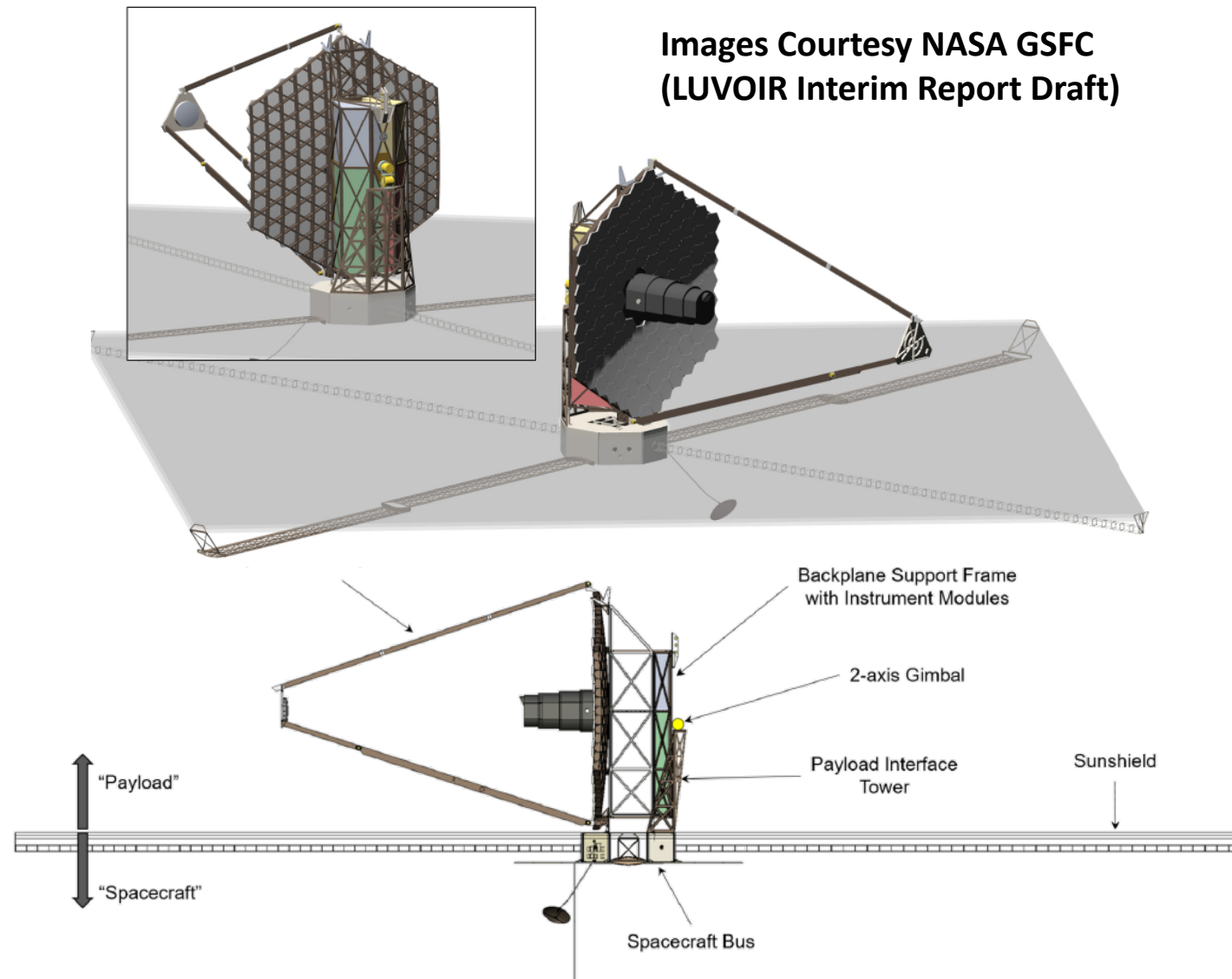


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# Key System-Level Requirements Relevant to Telescope LOS Pointing and Isolation – LUV O I R Architecture A



Specification	Req. Value
Dynamic wavefront error stability	Driven by coronagraph high-contrast requirements: $\leq 40$ pm (TBR) RMS WFE over $\sim 10$ minutes
Telescope pointing stability (@ OTE focal plane)	$< 0.3$ mas $1\sigma$ over an observation
Object tracking	$\leq 60$ mas/sec, object space
Slew rate	Repoint anywhere in anti-sun hemisphere in 45 minutes (Goal: 30 minutes)

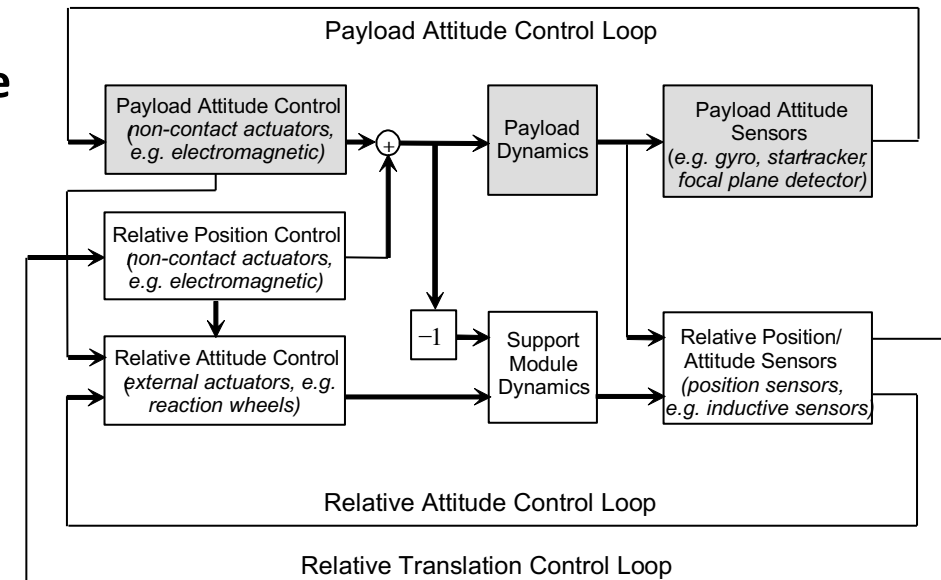
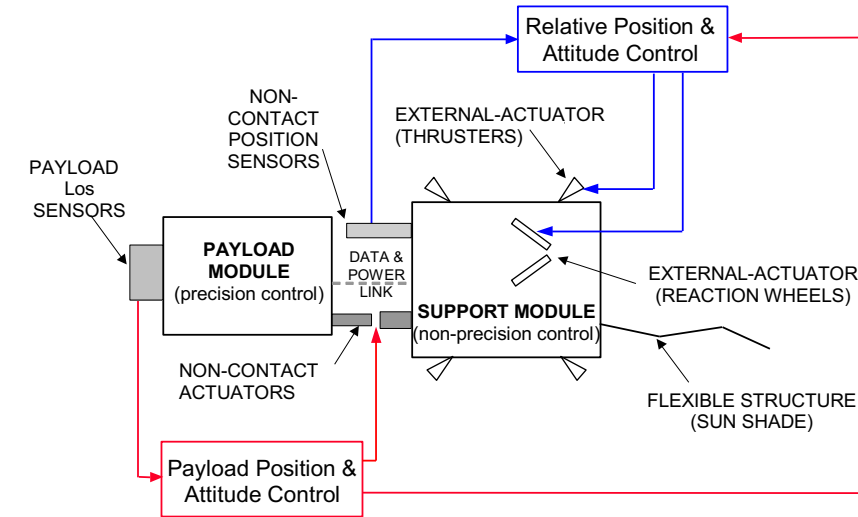




# Overview of a Canonical Non-Contact Pointing and Vibration Isolation System

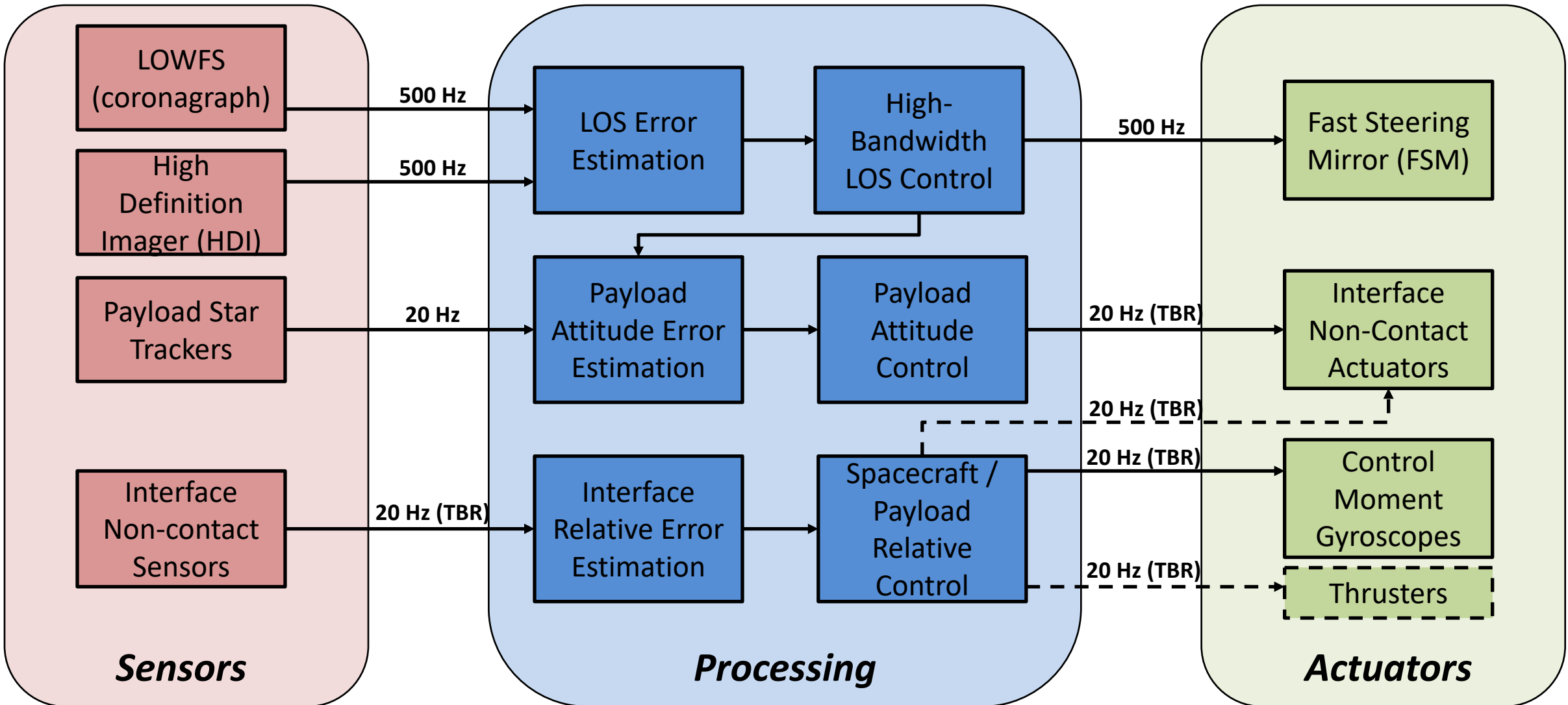


- **Non-contact vibration isolation technologies, like Lockheed Martin's Disturbance Free Payload (DFP), is an entirely novel concept for isolation of a sensitive science payload from the supporting spacecraft mechanisms**
  - *A DFP-configured spacecraft is actually two spacecraft flying in close formation*
- **The payload controls the telescope Line-of-Sight by pushing against the spacecraft inertia using a set of six non-contact Lorentz force actuators**
- **The spacecraft controls its inertial attitude such that interface stroke and gap are maintained**
  - Requirements for spacecraft attitude control are no more stringent than those for conventional spacecraft, and do not derive from payload pointing requirements
- **Payload Line-of-Sight isolation from Spacecraft disturbances is broadband, even down to low frequency, and is not affected by interface sensor measurement noise**



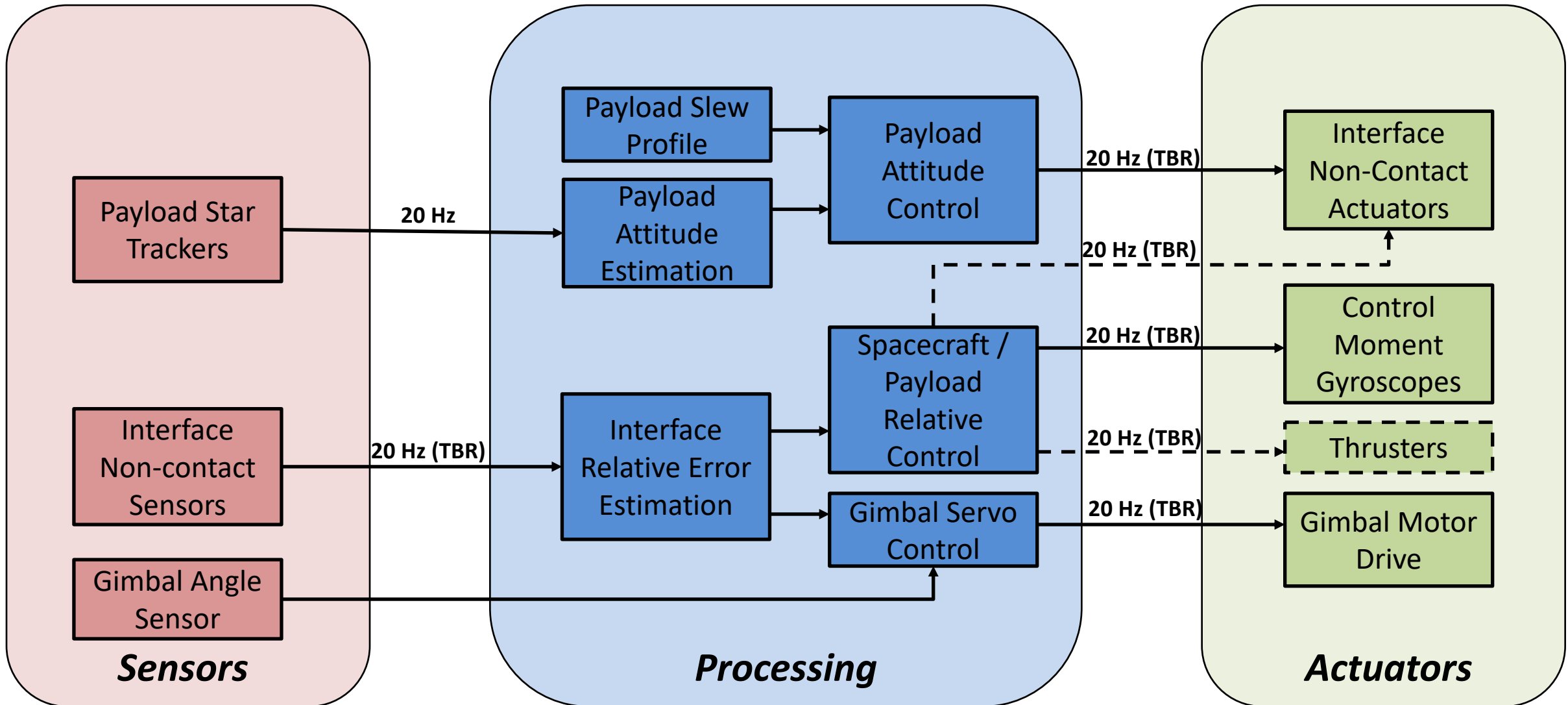


# Principal Signal Architecture: Steady-State Observatory Observation





# Principal Signal Architecture: Observatory Repointing and Slewing

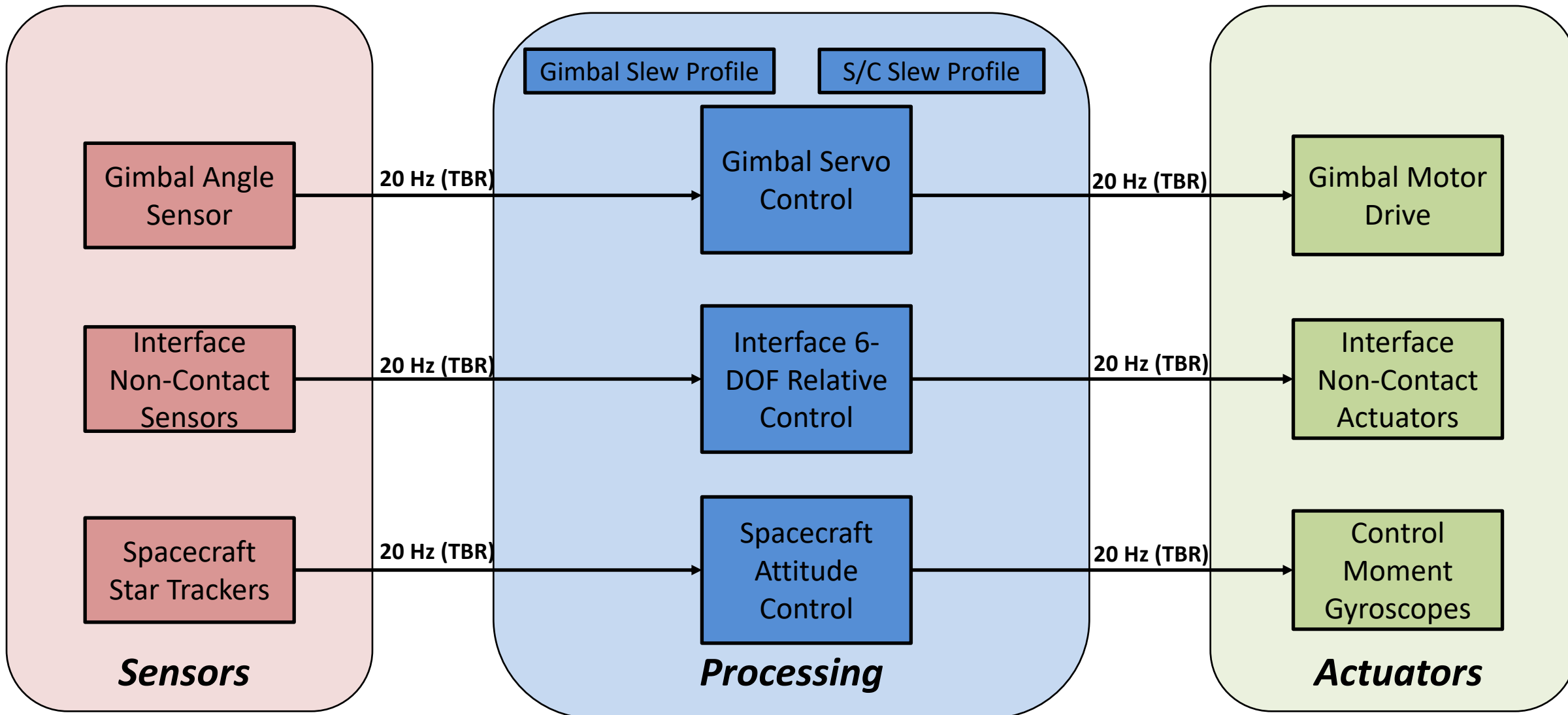




# Alternate Signal Architecture: Observatory Repointing and Slewing

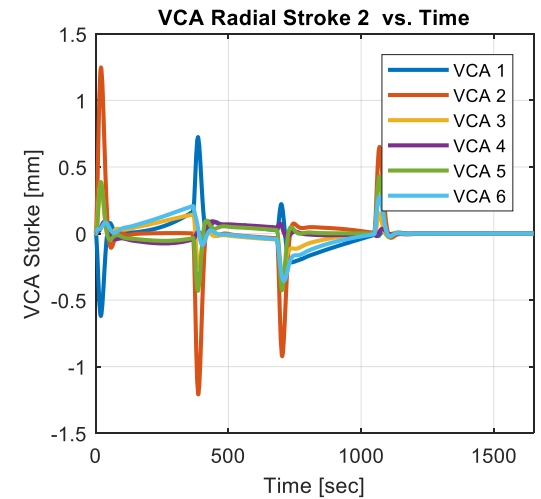
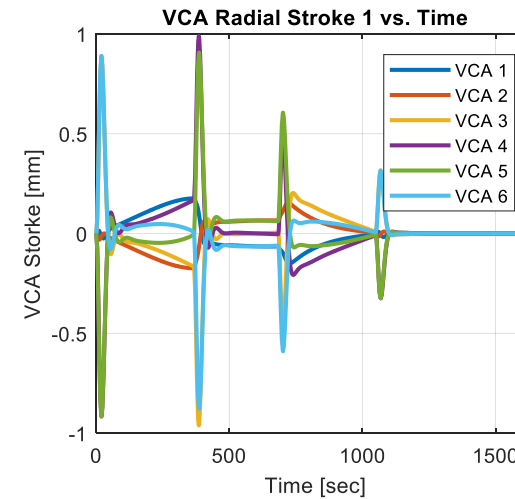
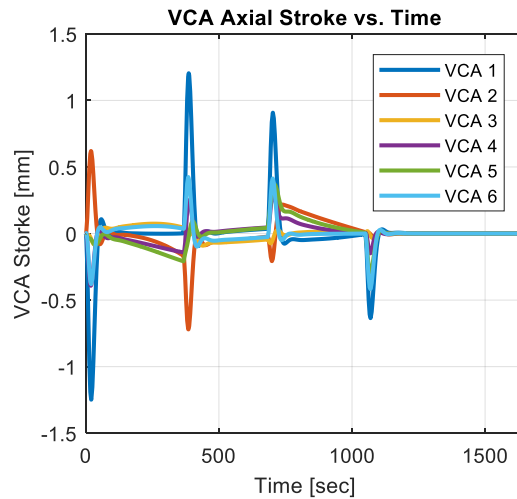
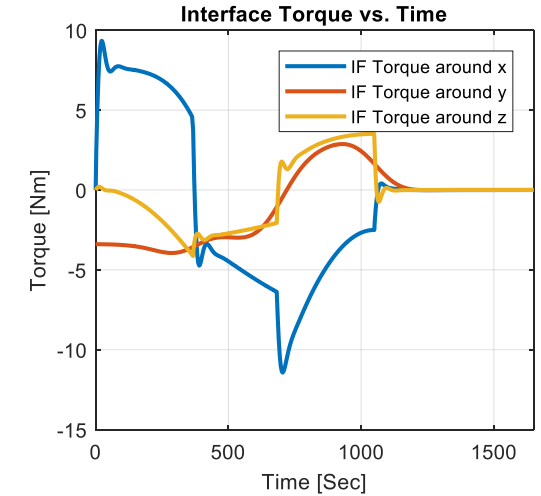
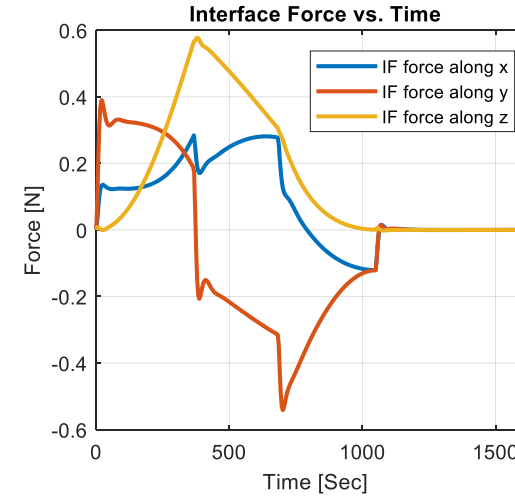
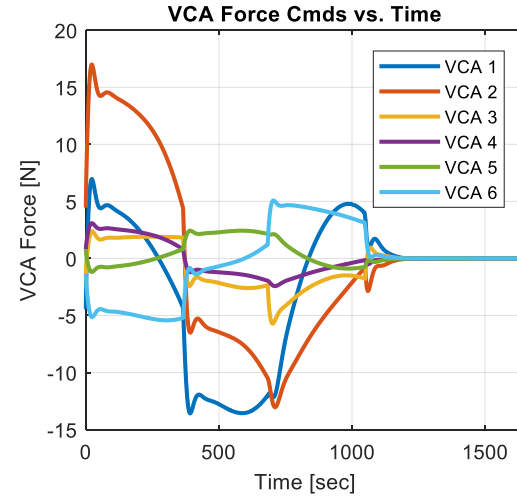
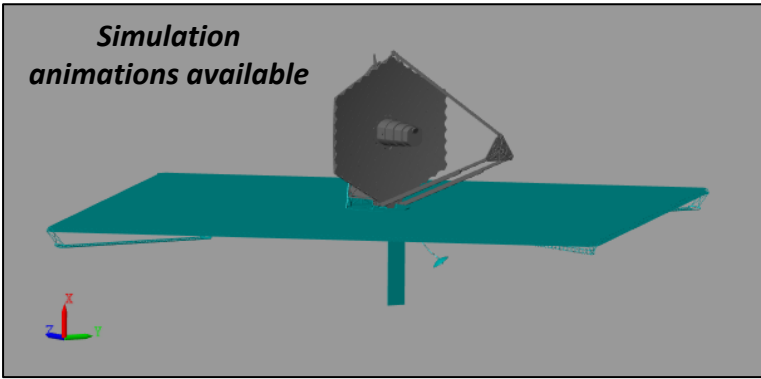


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# Nonlinear, Rigid-Body Simulation Results: LUVOIR repositioning with a non-contact interface



	Initial Angular Condition	Final Angular Condition
Spacecraft	0° around sun pointing axis (x axis)	180° around sun pointing axis (x axis)
Gimbal	90°	0°

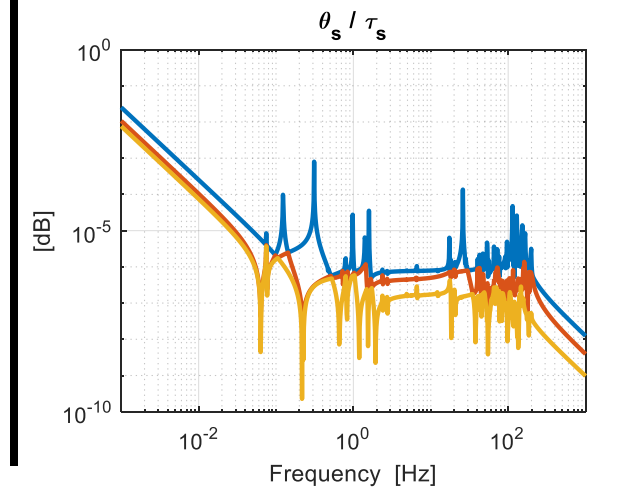
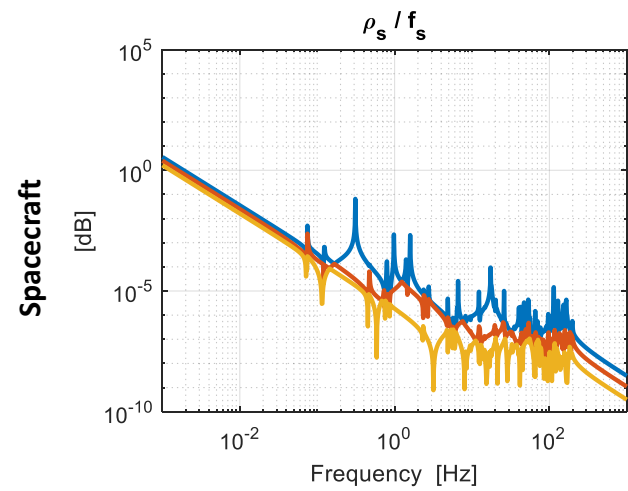
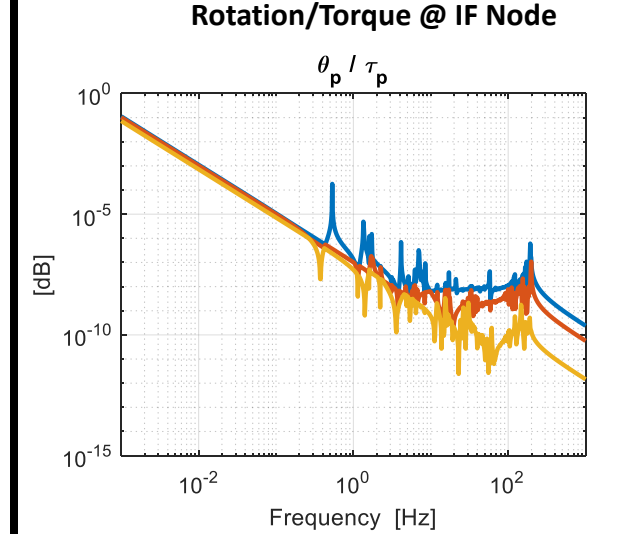
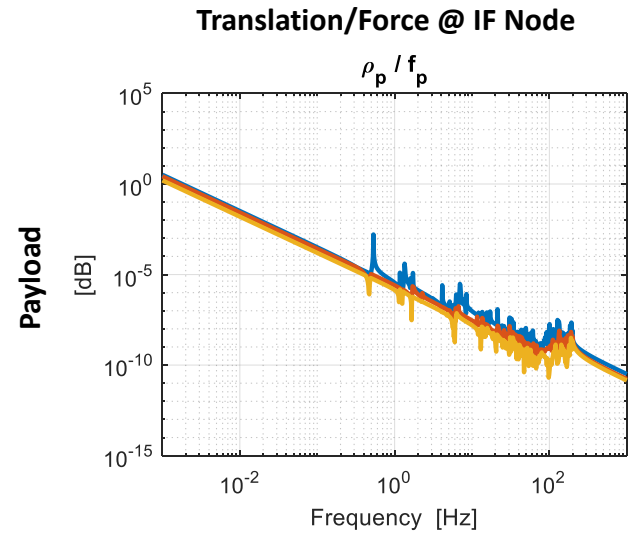
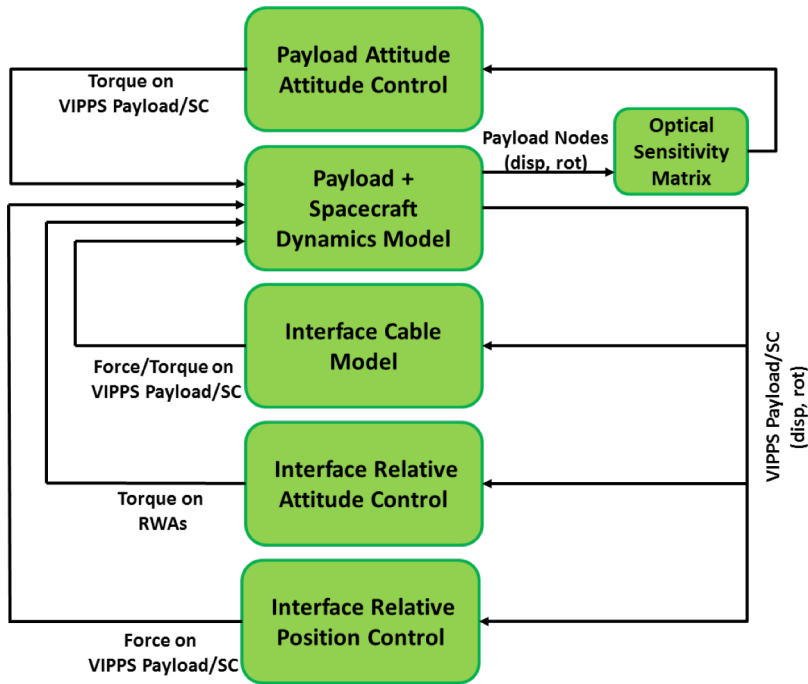
- Lockheed Martin's 10 mm VCA design can achieve the peak force and gap/stroke demands:
  - Max. VCA Force: 16.9 N
  - Max. Axial Gap: 1.24 mm
  - Max. Radial Gap: 1.24 mm
  - Max. Current: 3.08 A (per actuator)
  - Max. Power: 31.9 W (per actuator)

**Nonlinear dynamics simulations of multiple repositioning profiles shows that the non-contact interface can be maintained within gap and NCA force limits**





# Integrated Structure/Controls/Optics Modeling: an Early LUV O I R Architecture A Finite Element Model



- Structural dynamics model was extracted from a single FEM with two disconnected spacecraft and payload bodies
- Number of modes: 4373
- Model restrictions: monolithic PM, only LOS output from linear optical sensitivities (no WFE output)

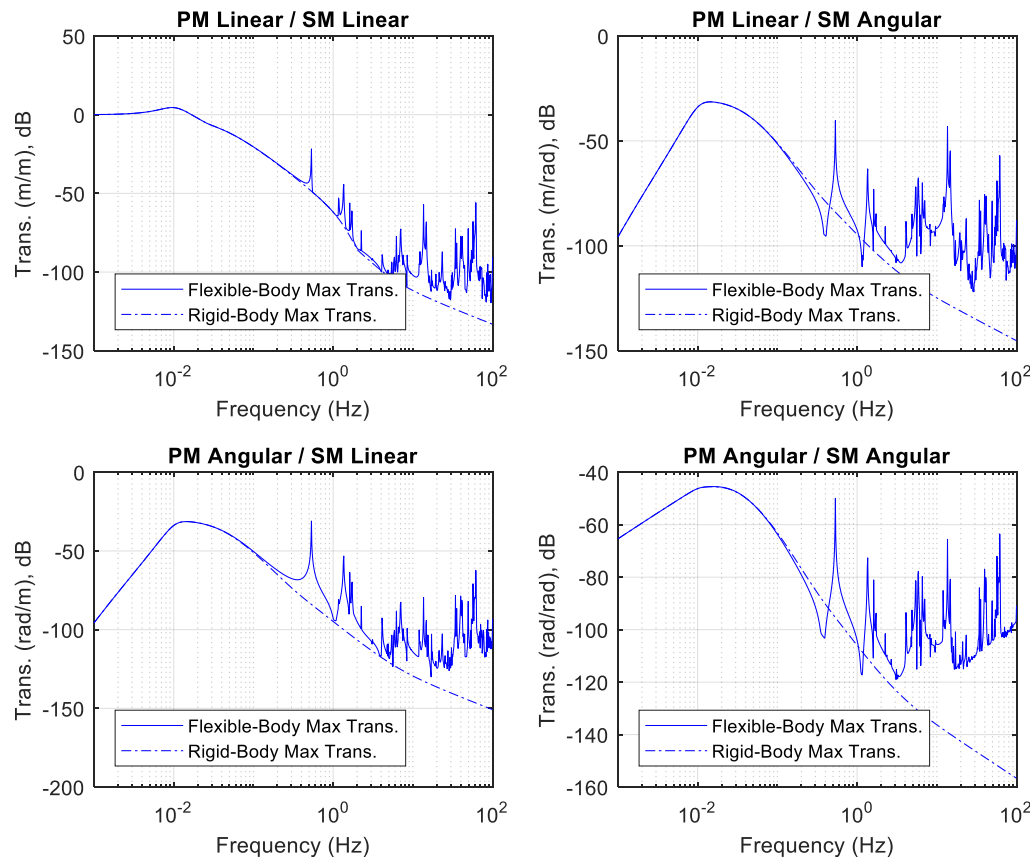
Early efforts of integrated controls/structure/optics modeling has yielded insights into LUV O I R dynamics and sharpened the process of further model integration activities



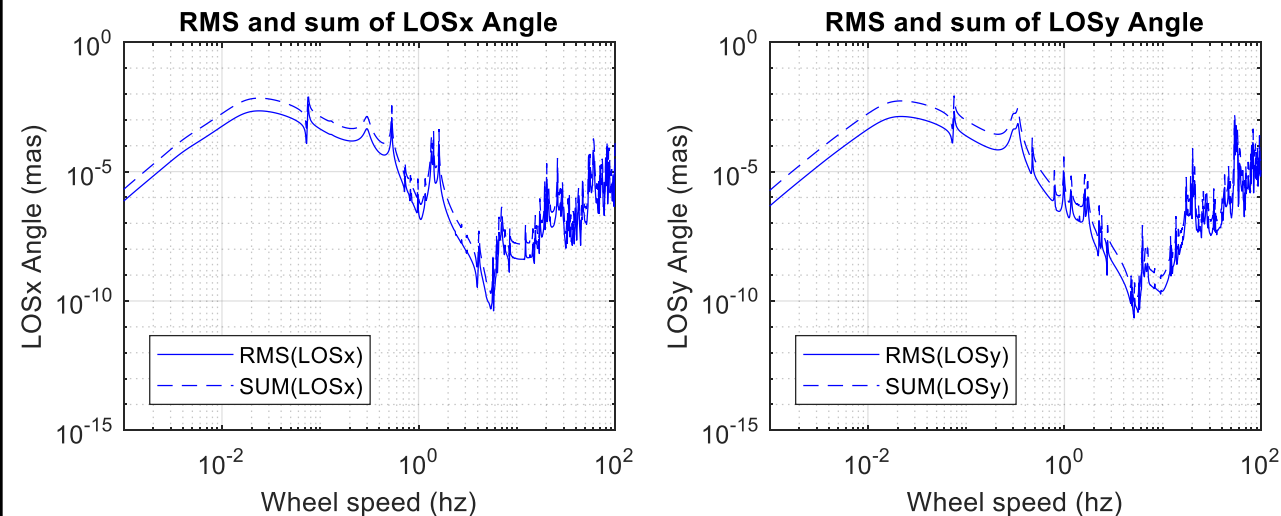
# Example closed-loop frequency-response results: steady-state science observation



- Spacecraft/payload interface transmissibility obtained
- Structural resonances in spacecraft or payload can have a significant effect on transmissibility
- Transmissibility is not a direct measure of system optical stability



- Initial simplified analysis of LOS error amplitude over a range of possible CMG rotor speeds:
  - assuming static and dynamic imbalance of the CMGs
  - Total LOS output was computed under two assumptions: (a) all 4 CMG imbalances are in phase (sum); (b) all 4 CMG imbalances have random phase (RMS)
- Forward work: consider CMG disturbance harmonics and contribution over all CMG gimbal angles





# I&T Concept Planning for Estimating

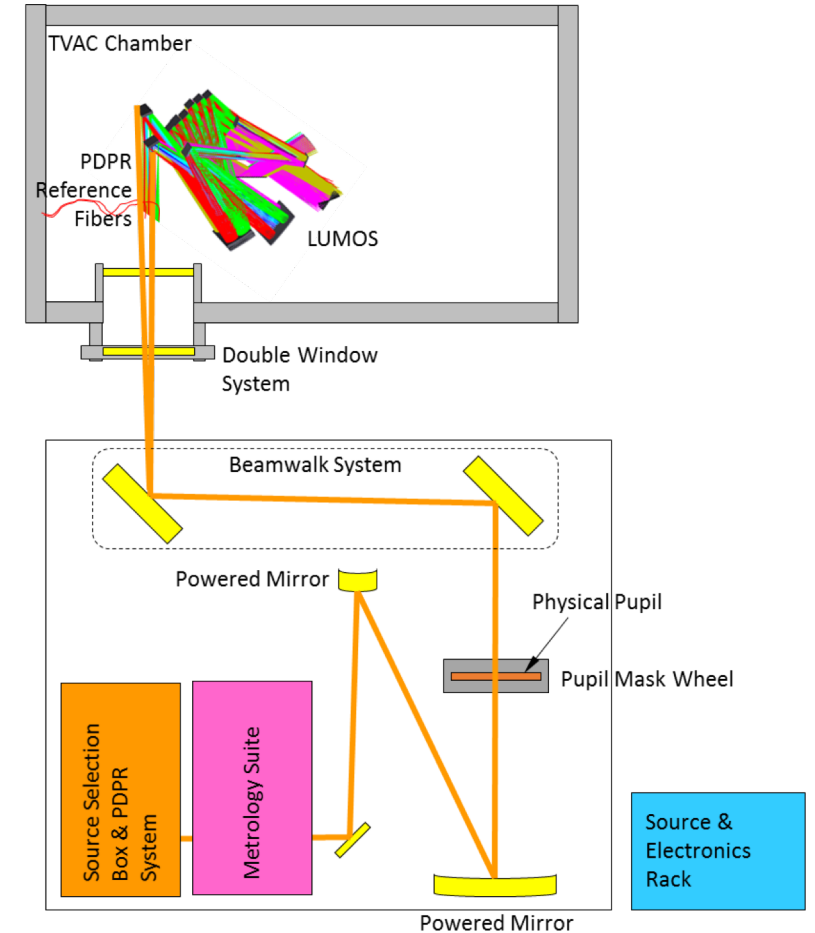
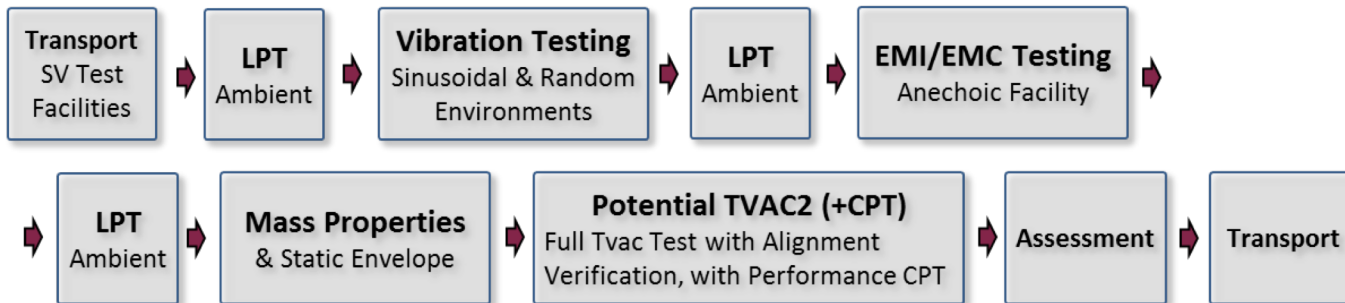


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## Establish sequence and timelines

- Establish nominal integration flow to assemble and perform baseline test at temperature and pressure efficiently. Validate predicts.
- Establish assembly sequences to reference, course align and fine align optical train. Design in reference fiducials for alignment efficiencies.
- Plan for surrogates, with capability for component remove/replace within spatial alignment.
- Once comprehensive baseline is established, execute environmental test program, using Limited Performance Tests throughout to track health, alignment and trending data.



LUMOS and ECLIPSE Test



# I&T Facilities Considerations for planning



## Facilities

Establish facilities required to Handle, Integrate, Test and Deliver two Large Optical Payload Assemblies. Desire to have best co-location to minimize transport and handling risk.

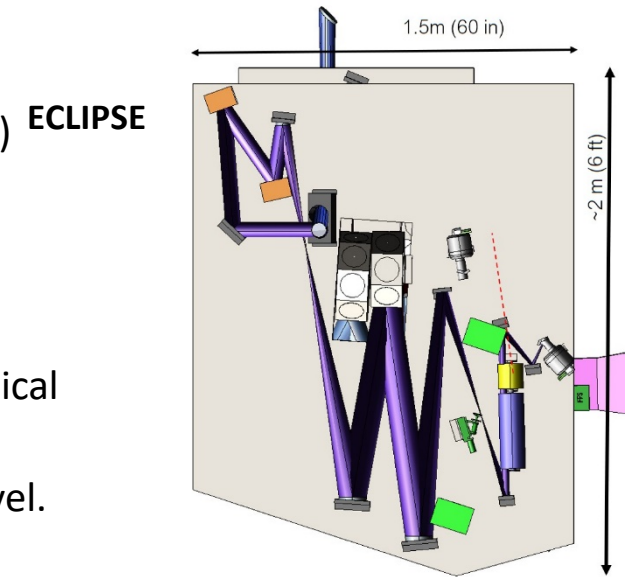
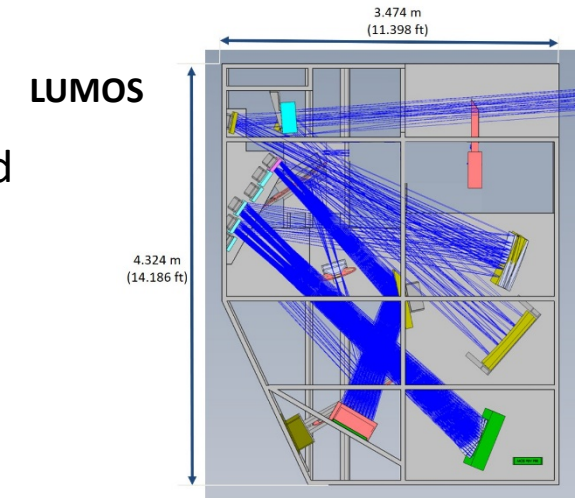
- LUMOS – Approximately 3.5 m (11.4 ft) x 4.3 m (14.2 ft)
- ECLIPS – Approximately 1.5 m (5 ft) x 2 m (6 ft)

## Integration Space Considerations

- Sufficient clean rooms with optical bench space capable of supporting sizes indicated
- Adjacent space to support optical test bed for alignments, optical train buildup and phase retrieval
- Handling/Crane Considerations, Logistical support considerations (precision clean, optics stores, etc)

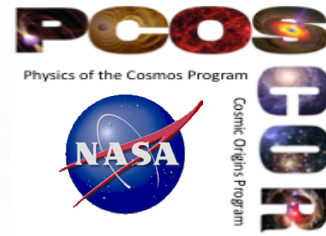
## Environmental Test Considerations

- TVac: Chamber large enough to accommodate LN shrouds, Helium Cyro Shrouds and Payloads.
- TVac: Chamber incorporates large enough optical window and adjacent floor space for external optical test bed sources, compound motion beam walking and other potential optical metrology.
- EMI: Anechoic Chamber large enough to accommodate, appropriate noise floor and cleanliness level.
- Vibe: Shaker system to meet size/mass and modal requirements of each system



# System-Level Segmented Telescope Design

PI: Larry D. Dewell/Lockheed Martin



## Objectives and Key Challenges:

- Address the system-level design challenges of large, UV/IR space telescopes to achieving picometer-level wavefront stability to support coronagraphy-based science
- Develop new testbeds to anchor picometer-class integrated models
- Inform NASA technology development plans to support large telescope missions in the 2020 Decadal Survey

## Significance of Work:

- Establish, through analysis and anchoring testbeds, engineering confidence in the feasibility of picometer stability for large telescopes

## Approach:

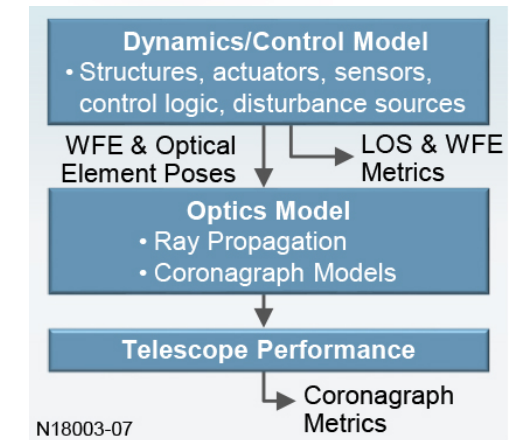
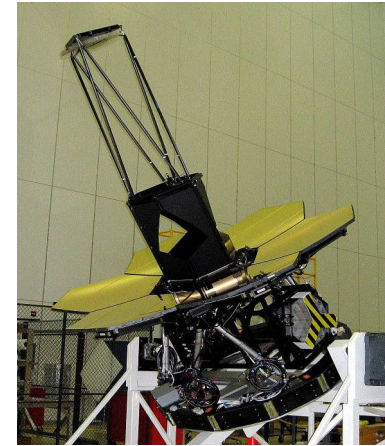
- Develop integrated telescope models to predict quasi-static and dynamic wavefront error performance from STDT initial models
- Anchor models and mature technology through testing under internal R&D funding

## Key Collaborators:

- Ray Bell and Alison Nordt – Lockheed Martin Advanced Technology Center
- Jay Daniel – Coherent Inc.
- Jeffrey Klingzahn – Harris Corp.
- Bari Southard – United Technologies Aerospace Systems (UTAS)

## Current Funded Period of Performance:

- April 2018 – April 2019



*Segmented Telescope Modeling, Anchored by Test*

## Recent Accomplishments:

- ✓ Notification of award: March 16, 2018
- ✓ Kickoff meeting: April 17, 2018

## Next Milestones:

- Baseline architecture performance complete, and mid-term review: September 2018
- Technology development plan: December 2018
- Final report: April 2019

## Application:

- Large Ultraviolet / Optical / Infrared (LUVOIR) Surveyor, Habitable Exoplanet Imaging Mission (HabEx), Origins Space Telescope (OST)



# Cooperative Agreement Progress Report Summary



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- **Key Program Points**

- Period of Performance has been extended at no cost to NASA to 7/31/2018
- Final report will summarize results of integrated modeling exercise, and Instrument AI&T plans

- **Key takeaways:**

- Through analysis, modeling and simulation, the CAN activity has shown that a non-contact payload/spacecraft isolation system is feasible for LUV O I R, meets the necessary agility requirements, and suggests excellent pointing and vibration isolation benefits to the architecture
- The CAN pointing and isolation integrated modeling has provided an early exercise in this integrated modeling approach which will be more further refined and exercised in the System-Level Segmented Telescope Design (SLSTD) follow-on efforts
- Requirements for LUV O I R Instrument Assembly, Integration and Test (AI&T) have been reviewed, a initial conceptual work flow concept is established, and further planning efforts are underway to support the CAN Final Report