

# Telescopes & Mirrors

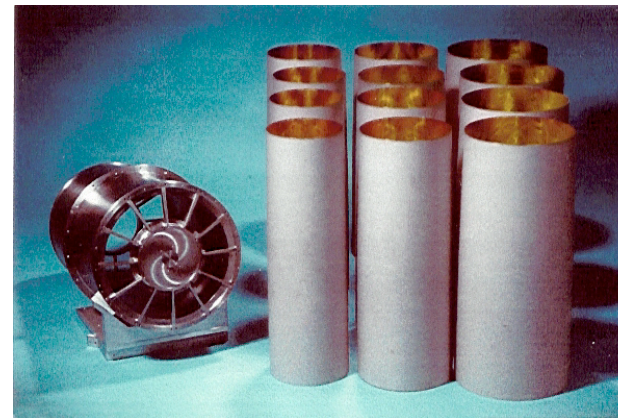
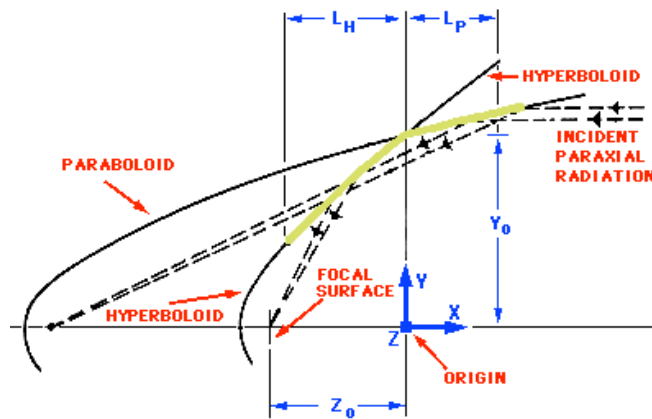
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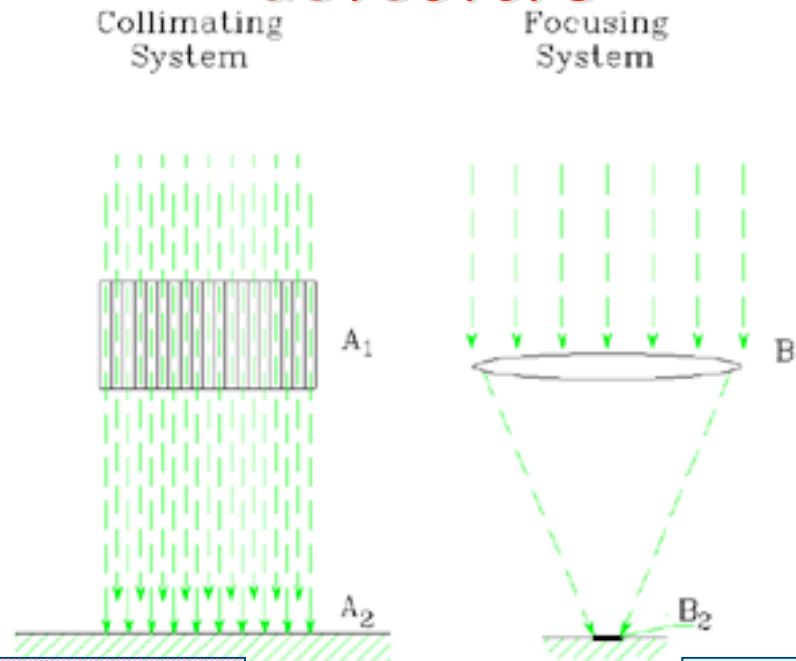
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# Outline

- ✓ remarks on grazing - incidence for X-ray astronomy
  - why grazing incidence reflection
  - optical configurations for grazing-incidence mirrors
- ✓ making mirrors
  - *the replication method*
- ✓ examples of past and future X-ray telescopes
- ✓ remarks on Gamma ray focusing telescopes and optics

# Advantages of focusing optics versus direct-view detectors



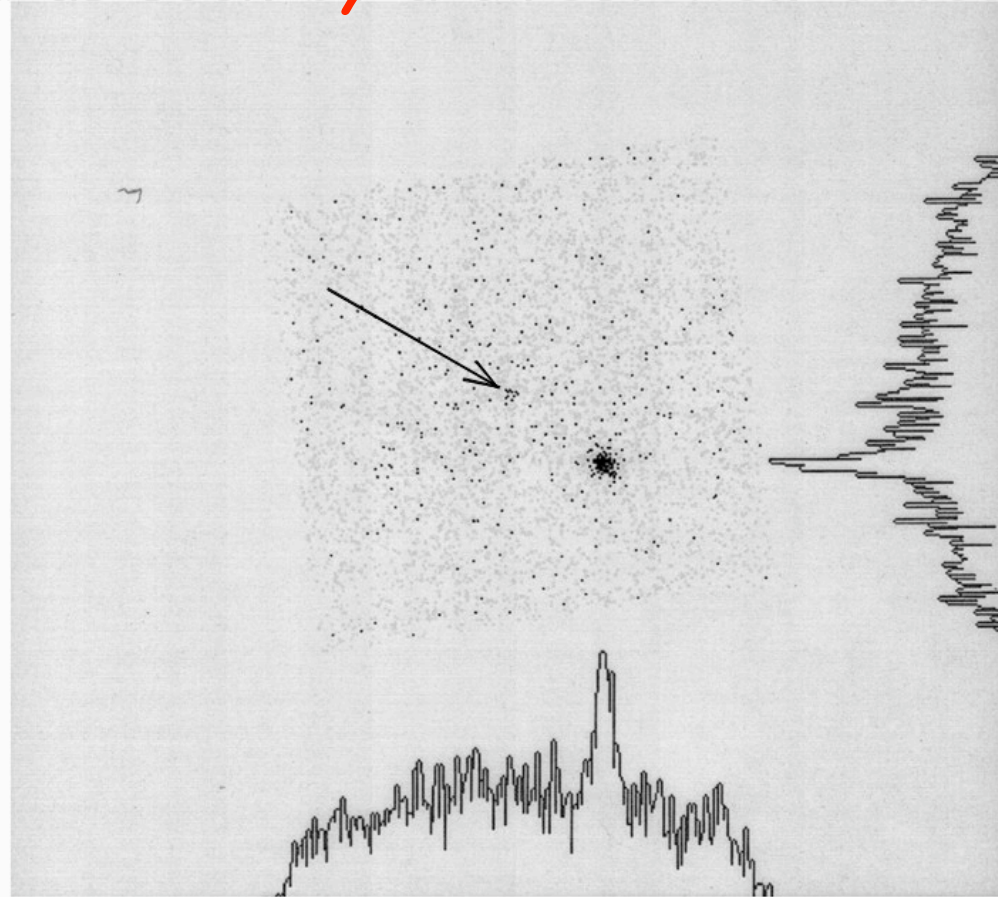
$$F_{\min} = n_{\sigma} \frac{\sqrt{2B}}{\sqrt{A_{\text{eff}} T_{\text{int}} \Delta E}}$$

$$F_{\min} = n_{\sigma} \frac{\sqrt{BA_d}}{A_{\text{eff}} \sqrt{T_{\text{int}} \Delta E}}$$

$B$  = background flux,  $T_{\text{int}}$  = integration time,  $\Delta E$  = integration bandwidth

Moreover: *much better imaging capabilities!*

*Simulation of two sources in a "Einstein" field as seen by a direct view detector*



With the direct vie detector the second "weak" sources is lost in the background

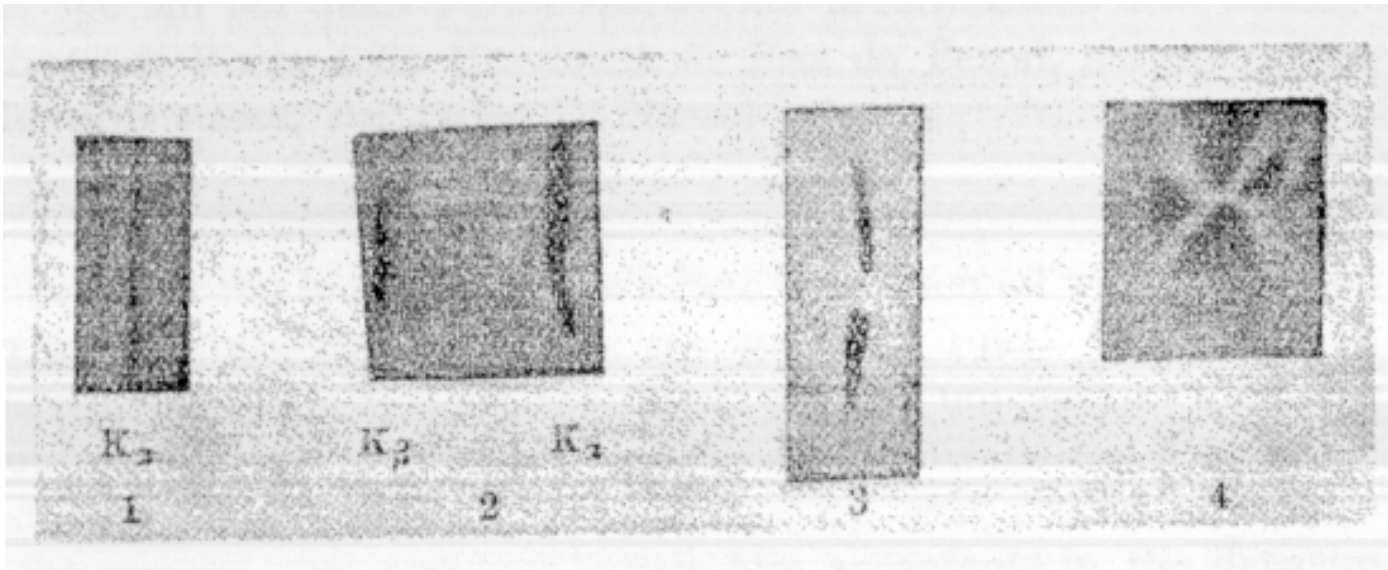
# *X-ray astronomical optics history in pills (I)*

- 1895: Roentgen discovers "X-rays"
- 1948: First successful focalization of an X-ray beam by a total-reflection optics (Baez)
- 1952: H. Wolter proposes the use of two-reflection optics based on conics for X-ray microscopy
- 1960: R. Giacconi and B. Rossi propose the use of grazing incidence optics for X-ray telescopes
- 1962: discovery by Giacconi et al. of Sco-X1, the first extra-solar X-ray source
- 1963: Giacconi and Rossi fly the first (small) Wolter I optics to take images of Sun in X-rays
- 1965: second flight of a Wolter I focusing optics (Giacconi + Lindsay)
- 1973: SKYLAB carry onboard two small X-ray optics for the study of the Sun

## *X-ray astronomical optics history in pills (II)*

- 1978: Einstein, the first satellite with optics entirely dedicated to X-rays
- 1983: EXOSAT operated (first European mission with X-ray optics aboard)
- 1990: ROSAT, first All Sky Survey in X-rays by means of a focusing telescope with high imaging capabilities
- 1993: ASCA, a multimodular focusing telescope with enhanced effective area for spectroscopic purposes
- 1996: BeppoSAX, a broad-band satellite with Ni electroformed optics
- 1999: launch of Chandra, the X-ray telescope with best angular resolution, and XMM-Newton, the X-ray telescope with most Effective Area
- 2004: launch of the Swift satellite devoted to the GRBs investigation (with aboard XRT)
- 2005: launch of Suzaku with high throughput optics for enhanced spectroscopy studies with bolometers

*Imaging experiments using Bragg reflection from  
"replicated" mica pseudo-cylindrical optics*



E. Fermi - Thesis of Laurea, "Formazione di immagini con i raggi Roentgen" ("Imaging formation with Roentgen rays"), Univ. of Pisa (1922)

Thanks to Giorgio Palumbo!

# X-ray optical constants

- complex index of refraction to describe the interaction X-rays /matter:

$\delta$  → changes of phase

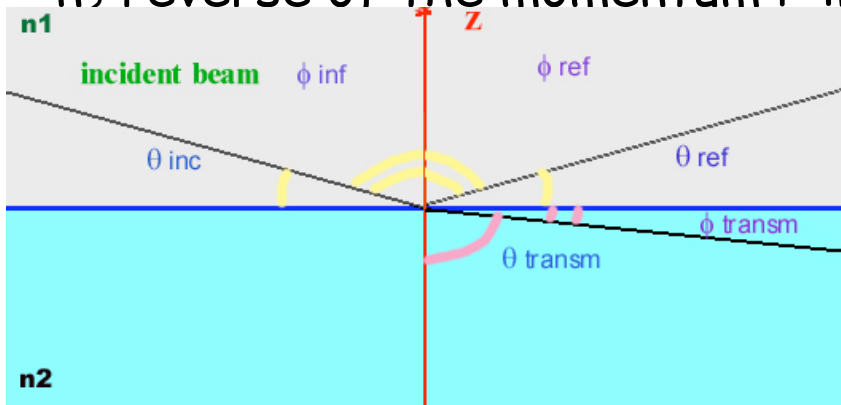
$\beta$  → absorption

$$\tilde{n} = n + i\beta = 1 - \delta + i\beta$$

$$(\mu = 4\pi\beta/\lambda \text{ cm}^{-1})$$

Linear abs. coeff.

- at a boundary between two materials of different refraction index  $n_1$ ,  $n_2$ , reverse of the momentum  $P$  in the  $z$  direction:



$$\vec{p}_1 = \frac{h}{2\pi} \vec{k}_1$$

$$|\vec{k}_1| = \frac{2\pi}{\lambda} n_1$$



$$2p_z \propto \frac{4\pi}{\lambda} n_1 \sin\theta_{inc}$$

momentum transfer

- the amplitude of reflection is described by the Fresnel's equations:

$$r_{12}^s = \frac{n_1 \sin\theta_1 - n_2 \sin\theta_2}{n_1 \sin\theta_1 + n_2 \sin\theta_2}$$

$$r_{12}^p = \frac{n_1 \sin\theta_2 - n_2 \sin\theta_1}{n_1 \sin\theta_2 + n_2 \sin\theta_1}$$



# Total X-ray reflection at grazing incidence

- if vacuum is material #1 ( $n_1 = 1$ )  $\rightarrow$  the phase velocity in the second medium increases  $\rightarrow$  beam tends to be deflected in the direction opposite to the normal.
- Snell's law ( $n_1 \cos\theta_1 = n_2 \cos\theta_2$ ) to find a critical angle for total reflection:

$$\theta_{crit} \approx \sqrt{2\delta} = \sqrt{\frac{r_0 \lambda^2 \rho N_{Av} f_1}{A\pi}}$$

$\lambda$  = wavelenght     $\rho$  = density  
 $A$  = atomico weight     $f_1$  = scattering coeff.  
 $r_0$  = classical electron radius

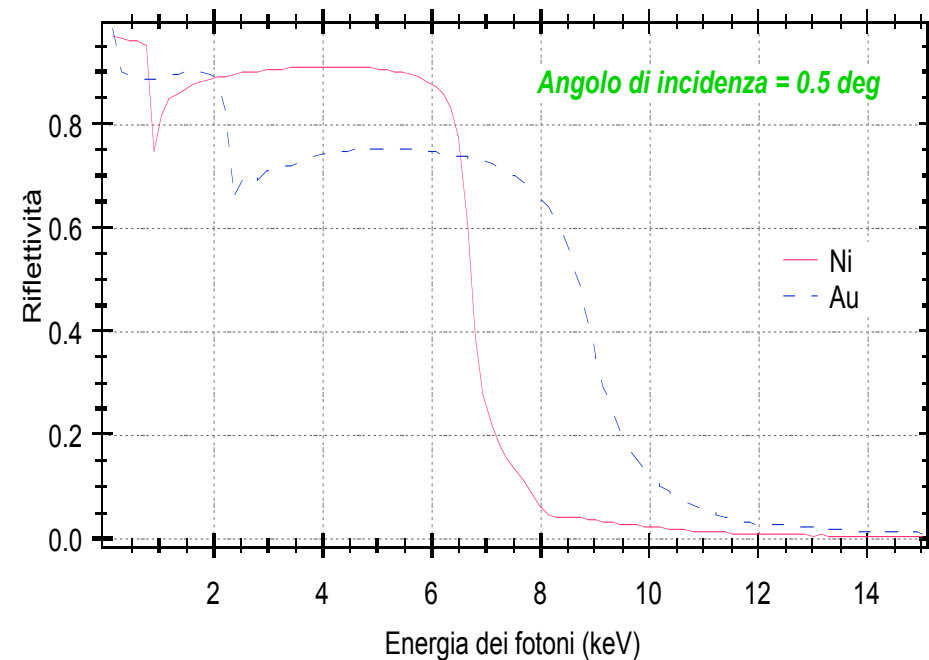
- far from the fluorecence edges  $f_1 \approx Z$  and for heavy elements  $Z/A \approx 0.5$ :

$$\theta_{crit} (\text{arc min}) \approx 5.6 \lambda (A) \sqrt{\rho}$$

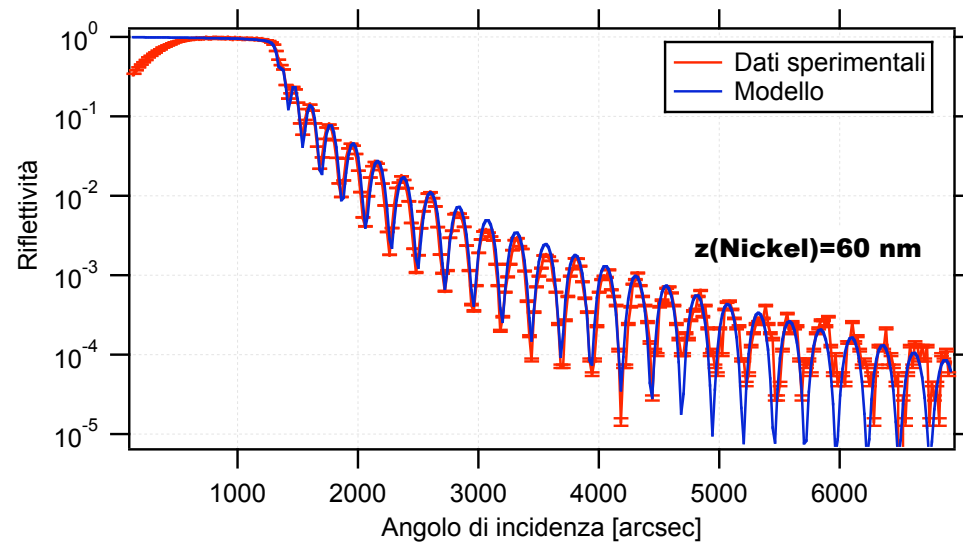
- reflectivity loss due to scattering:

$$I_R = I_0 \exp \left[ - \left( \frac{4\pi \cdot n \cdot \sigma \cdot \sin\theta}{\lambda} \right)^2 \right]$$

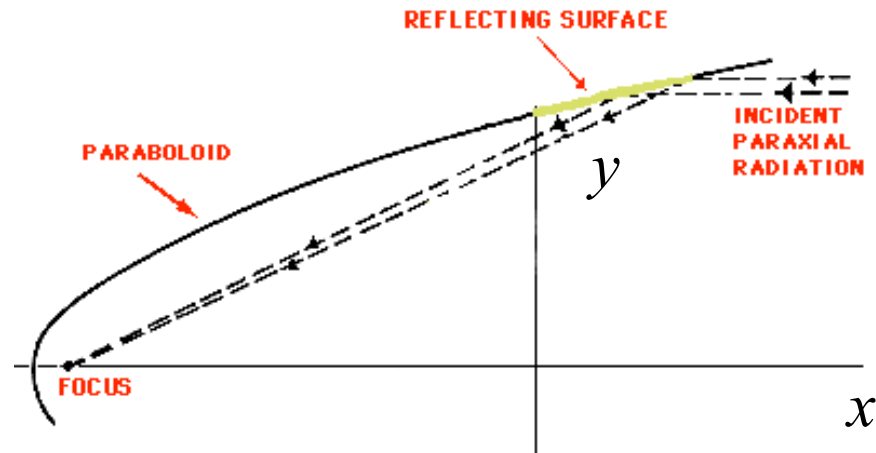
$\sigma$  = rms microroughn. level



## Other examples: C, Ni, Au



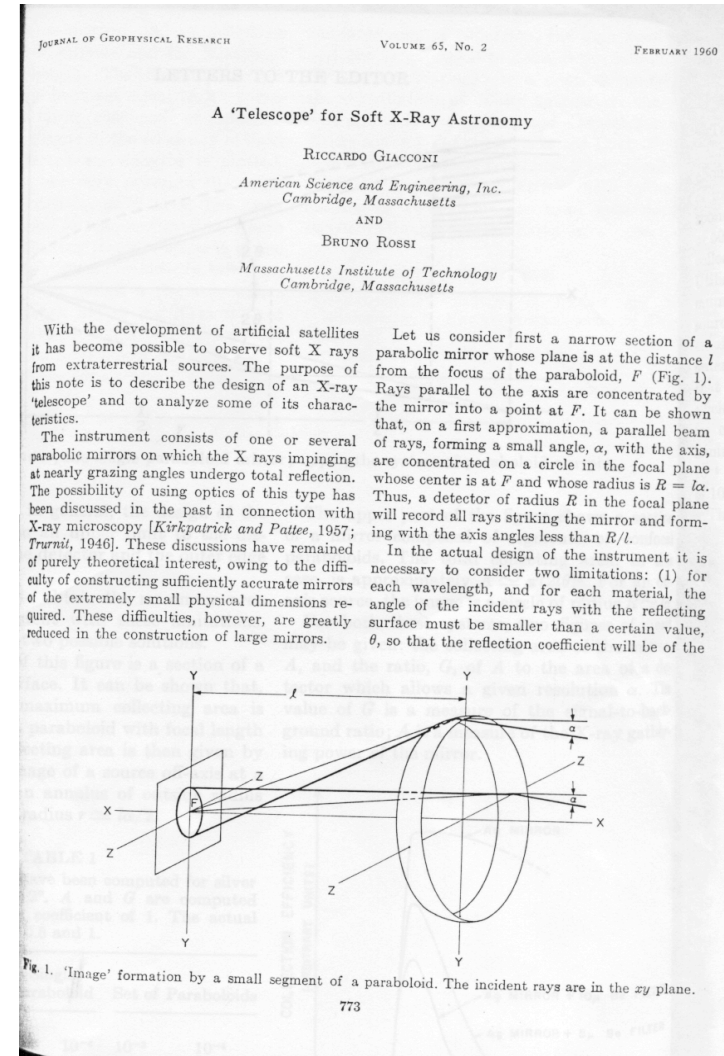
# X-ray mirrors with parabolic profile



$$y^2 = 2 p x$$

$$p = 2 * \text{dist. focus-vertex}$$

- perfect on-axis focusing
- off-axis images strongly affected by coma



# The Abbe sine condition to have coma-free focusing mirrors

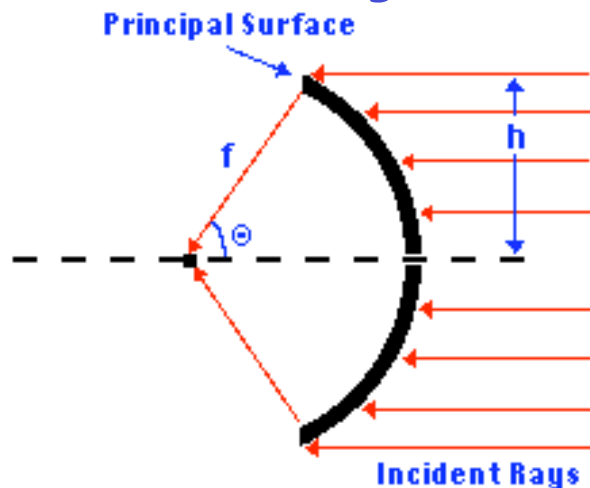
**Coma:** off-axis aberration caused by a different magnification of reflected rays, depending on the hitting position at the mirror surface



Typical blurring of a focal spot due to coma

➤ Coma free mirrors must satisfy the Abbe sine condition:

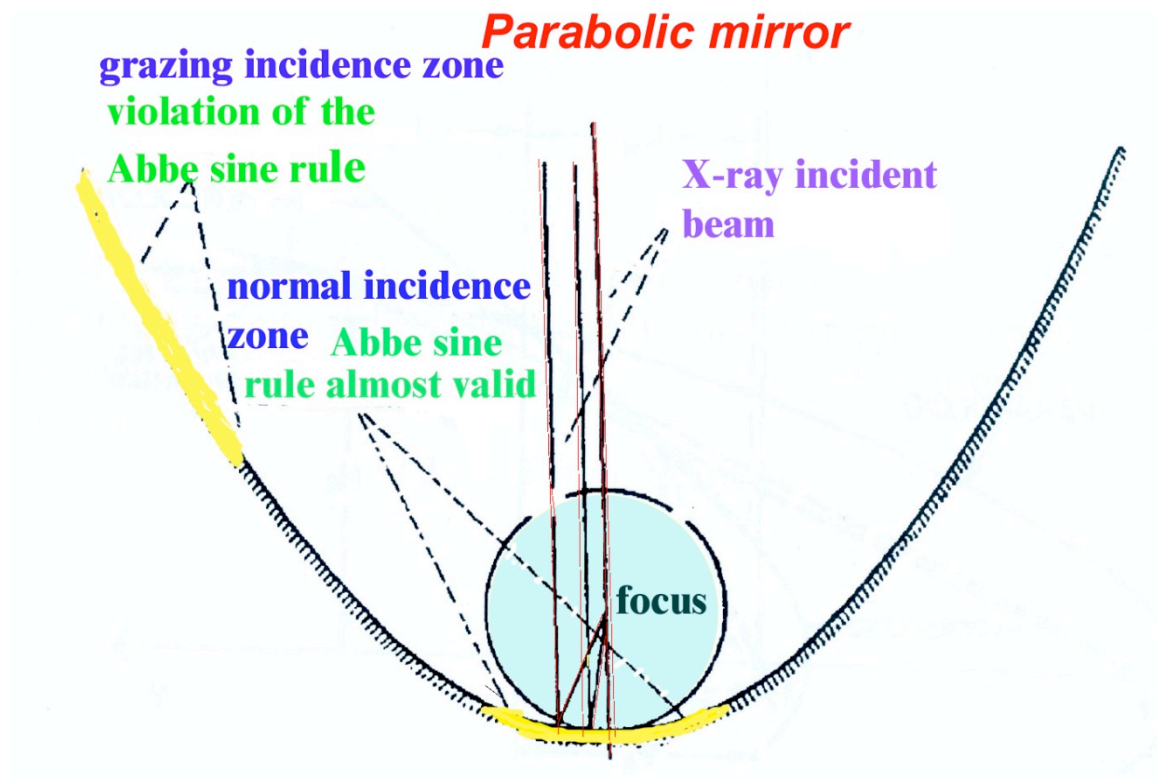
The surface defined by the intersection of each input ray with its corresponding output ray (principal or Abbe surface) must be a sphere around the image, i.e.:



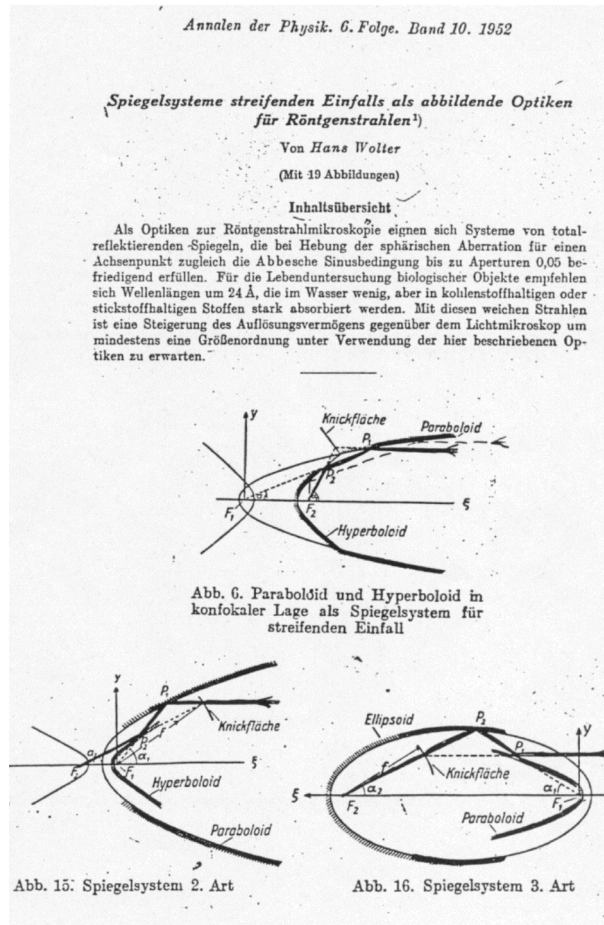
$$\frac{h_1}{\sin \theta_1} = \frac{h_2}{\sin \theta_2} = \text{const.}$$

# Parabolic mirrors & the Abbe sine condition

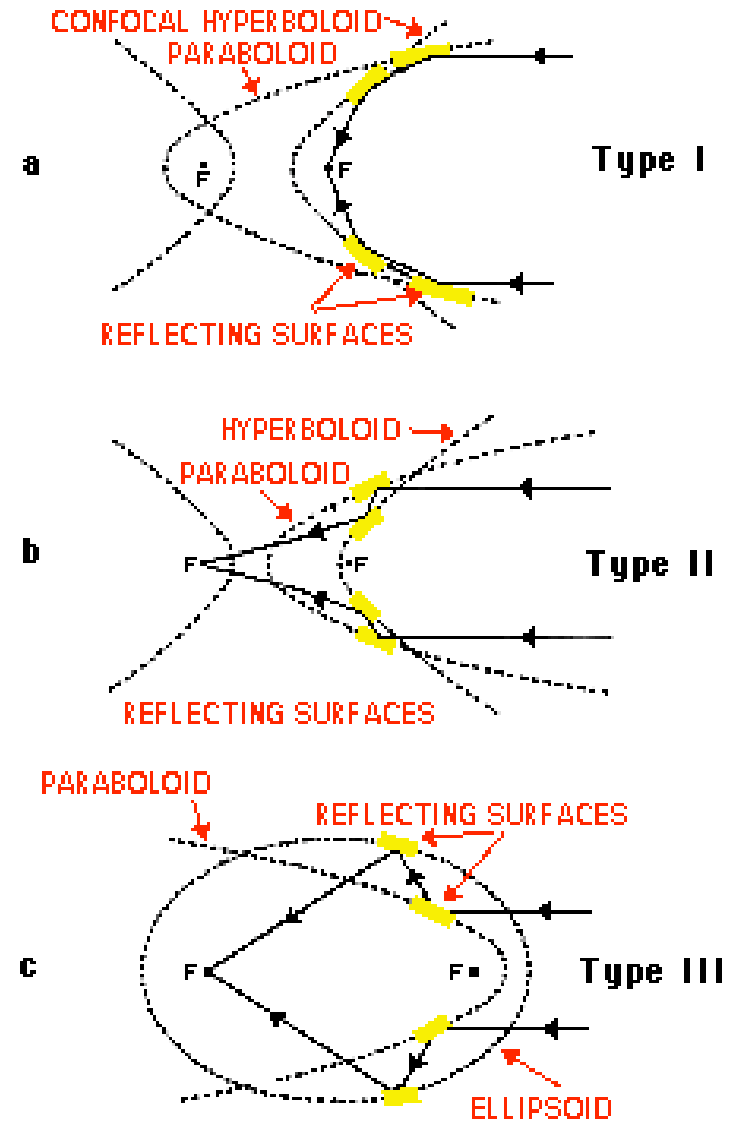
The parabolic profile approximately obeys to the Abbe rule only near the vertex, i.e. at normal incidence but not for grazing incidence angles  
→ the parabolic geometry is not optimal for X-ray telescopes



# Wolter's solution to the X-ray imaging



H. Wolter, Ann. Der Phys., NY10,94

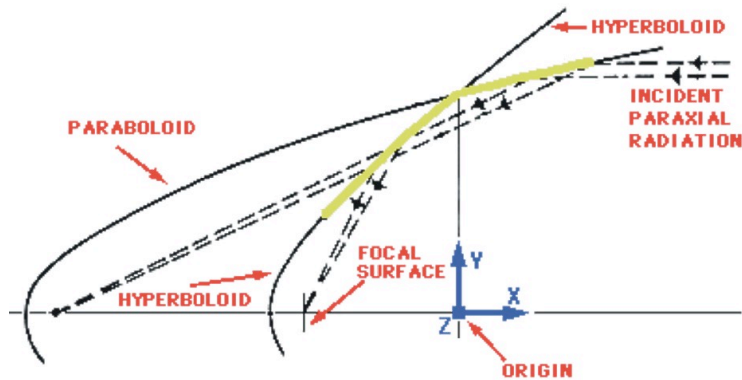


# The Wolter I mirror profile for X-ray astronomy applications

- it guarantees the minimum focal length for a given aperture

- it allows us to nest together many confocal mirror shells

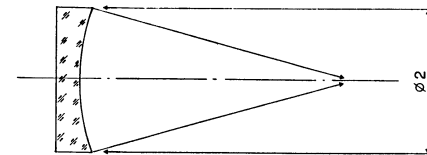
- Effective Area:  $8 \pi F L \theta^2 \text{Refl.}^2$



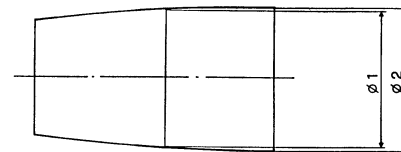
$F = \text{focal length} = R / \tan 4\theta$

$\theta = \text{on-axis incidence angle}$

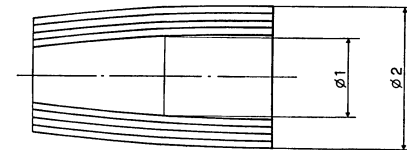
$R = \text{aperture radius}$



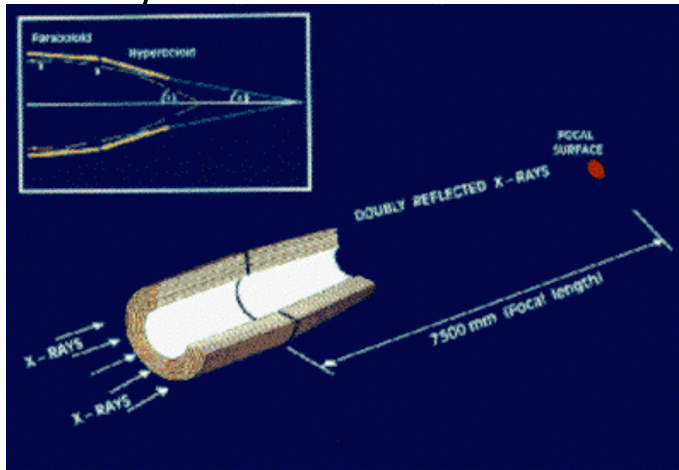
$$S_v = \frac{\pi \phi_2^2}{4}$$



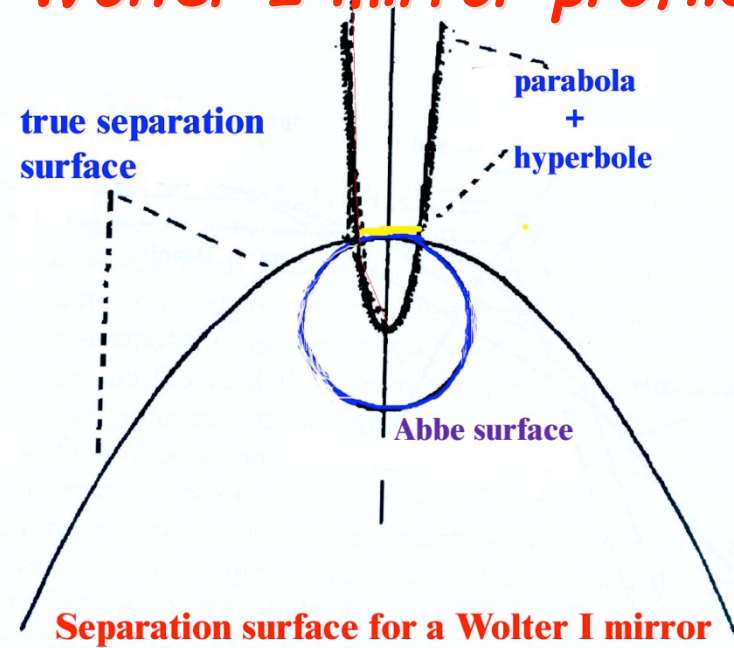
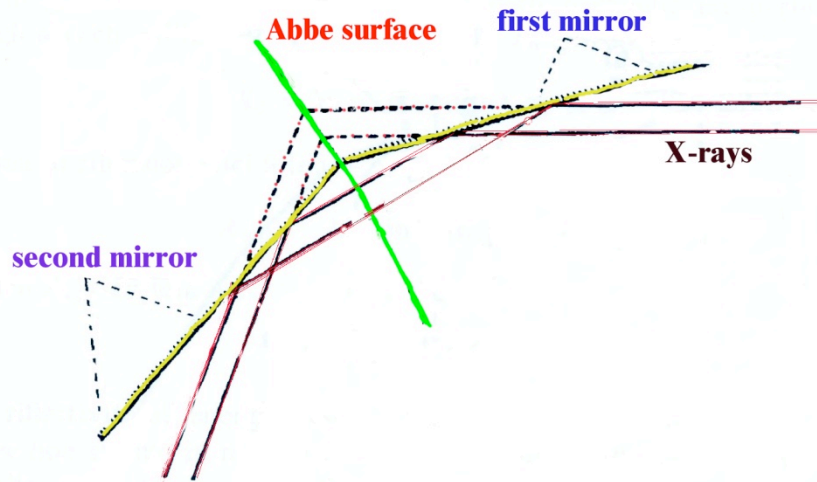
$$S_1 = \frac{\pi (\phi_2 - \phi_1)^2}{4}$$



$$S_x = \frac{\pi (\phi_2 - \phi_1)^2}{4}$$



# The Abbe condition and the Wolter I mirror profile



*Spherical aberration term*

**Separation surface for a Wolter I mirror**

$$\sigma_{rms} = 0.2 \frac{\tan^2 \gamma}{\tan \theta} \left( \frac{L}{F} \right) + 4 \tan \gamma \tan^2 \theta$$

*Residual coma term*

$\sigma_{rms}$  = rms blur circle  
L = mirror height

$\theta$  = incidence angle  
F = focal length

$\gamma$  = off-axis angle

## NOTE:

*the optimal focal plane is not flat:*  $\delta_{flat} \propto r^2 \frac{L}{F^2} \frac{1}{\tan^2 \theta}$  *r = focal plane radius*



## *Alternative profiles derived from Wolter I*

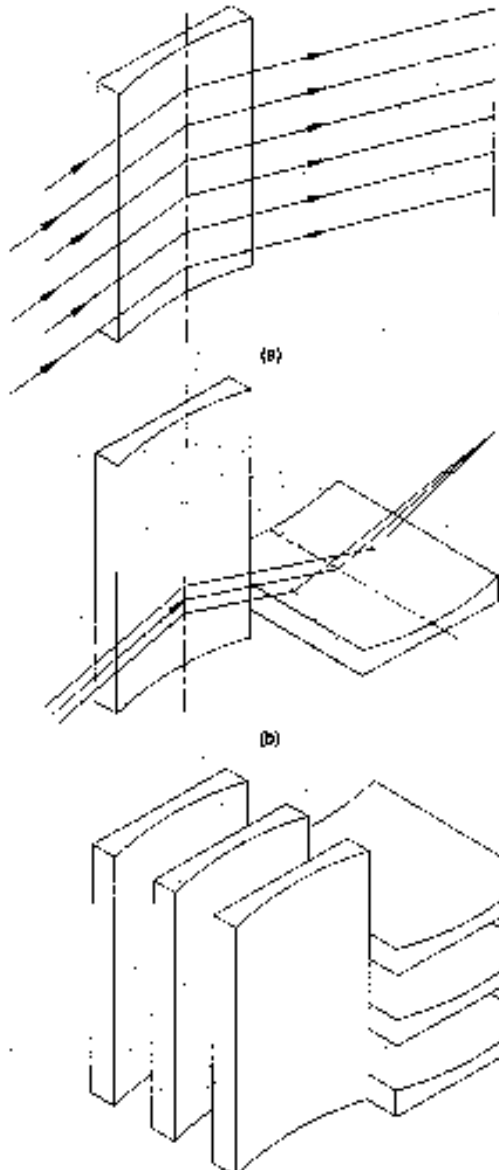
➤ Wolter-Schwarzschild profile: *it exactly satisfies the Abbe sine condition and it has been adopted for the Einstein mirrors; is coma free but it strongly affected by spherical aberration*

➤ double-cone profile: *it better approximates the Wolter I at small reflection angles: It is utilized for practical reasons (- cost + effective area). Intrinsic on-axis focal blurring given by:*

$$HEW \propto \frac{LR}{F^2}$$

➤ **polynomial** profile: *parameters have been specifically optimized to maintain the same HEW in a wide field of view*

*(introducing small aberration on-axis the off-axis imaging behavior is improved → same principle of the Ritchey-Chretienne normal-incidence telescope in the optical band)*



## **Kirpatrick-Baez Telescopes**

- *parabolic-profile curved mirrors in just one direction → to focus a beam in a single point another identical mirror has to be orthogonally placed with respect to the first one;*
- *it is possible to nest many confocal mirrors to increase the effective area;*
  - *compared to a Wolter I system with same focal length and same incidence angle (on-axis), angles are two time larger;*
  - *imaging capabilities result to be limited by some inherent aberration;*

*NB: by means of a K-B optics was performed the first successful attempt of the focalization of an X-ray beam in total-reflection regime (1948)*

# Lobster-Eye optics



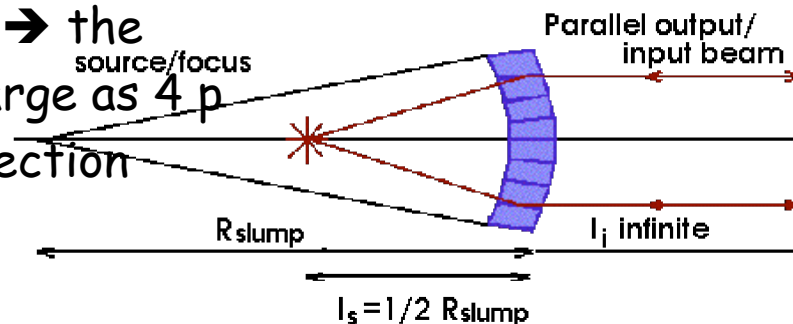
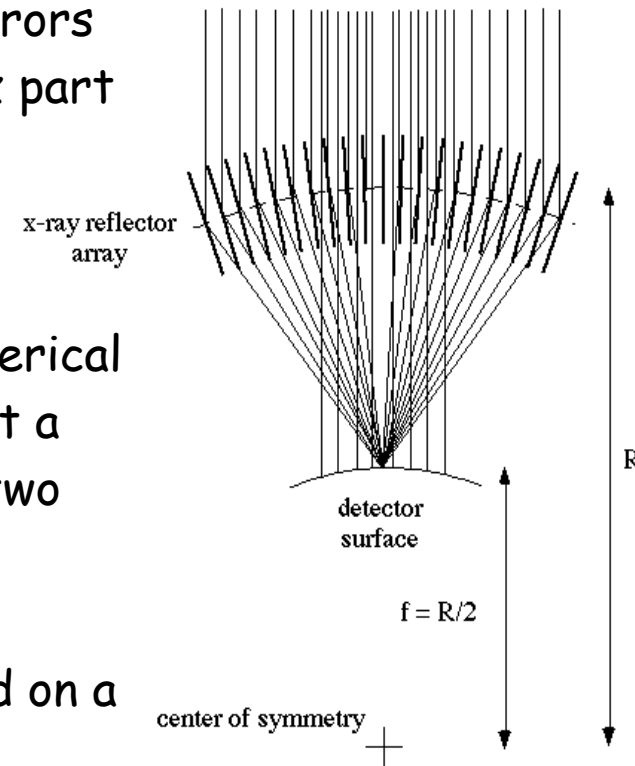
## Lobster-Eye Optics Geometry (1-dimensional)

➤ system similar to spherical normal-incidence mirrors but, in this case, the beam impinges on the convex part of the entrance pupil;

➤ the pupil is formed by a system of channels with square section uniformly distributed around a spherical surface of radius  $R$ . To be focused in a single point a collimated beam has to sustain the reflection by two orthogonal walls of a same channel;

➤ the photons are focused onto points distributed on a spherical surface of radius  $R/2$ ;

➤ a preferential optical axis does not exist → the system field of view can be in principle as large as  $4\pi$  with the same Effective Area for every direction





Credits: NASA

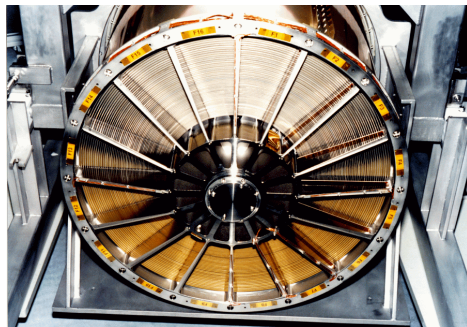
## Manufacturing techniques utilized so far

### 1. Classical precision optical polishing and grinding

Projects: **Einstein, Rosat, Chandra**

Advantages: *superb angular resolution*

Drawbacks: *high mirror walls → → small number of nested mirror shells, high mass, high cost process*



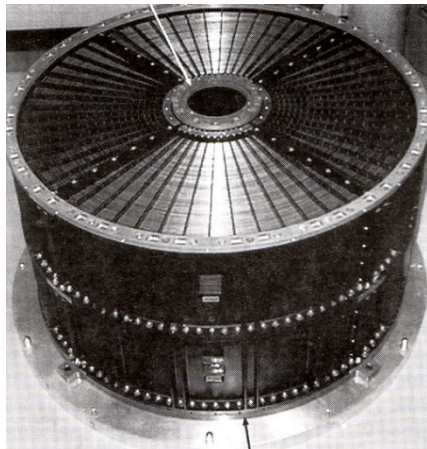
Credits: ESA

### 2. Replication

Projects: **EXOSAT, SAX, JET-X/Swift, XMM, ABRIXAS** (→ *examples follow hereafter*)

Advantages: *good angular resolution, high mirror “nesting” the same mandrels for many modules*

Drawbacks: *relatively high cost process; high mass/geom. area ratio (if Ni is used).*



Credits: ISAS

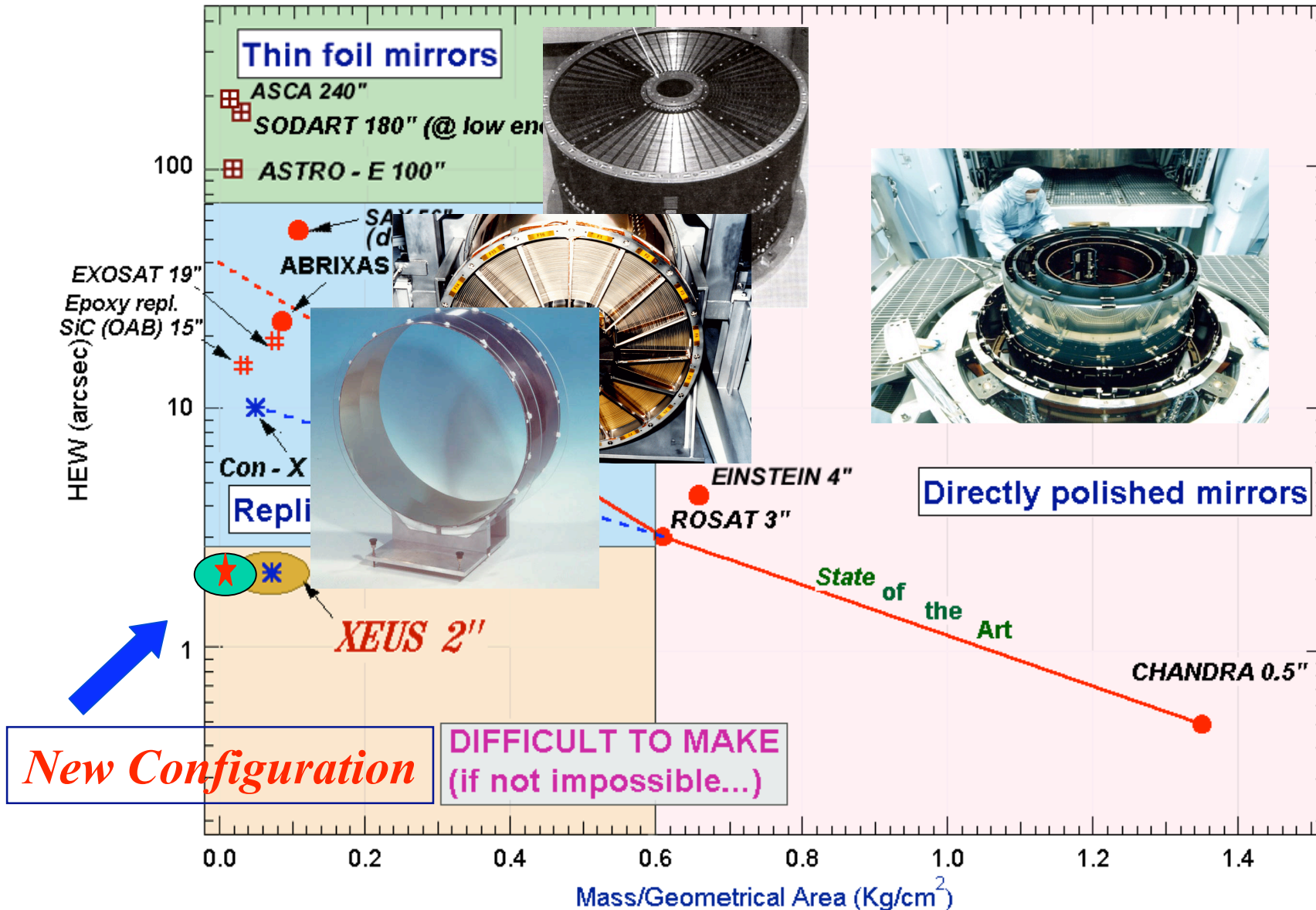
### 3. “Thin foil mirrors”

Projects: **BBXRT, ASCA, SODART, ASTRO-E**

Advantages: *high mirror “nesting” possibility, low mass/geom. area ratio (the foils are made of Al), cheap process*

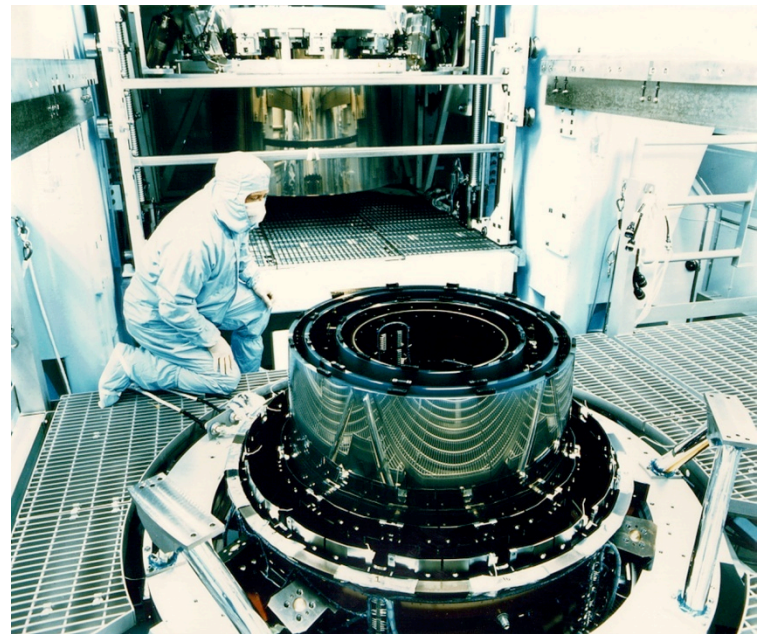
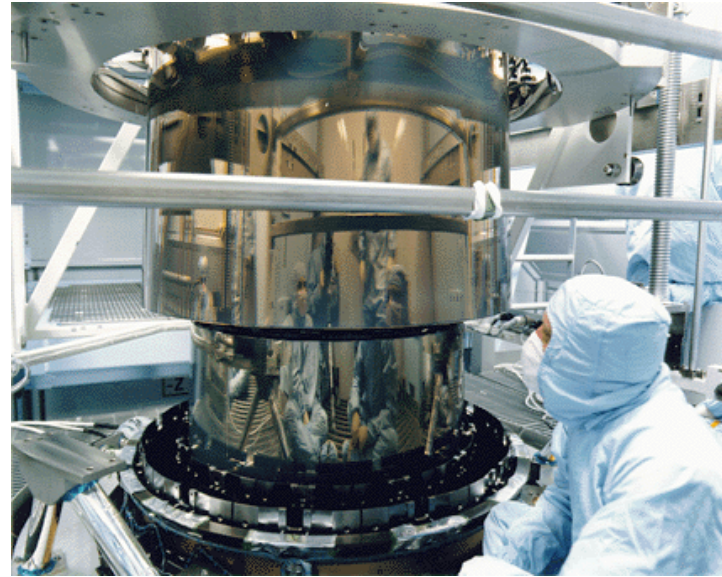
Drawbacks: *until now low imaging resolutions (1-3 arcmin)*

# Present Astronomical optics technologies: HEW Vs Mass/geometrical area



# Chandra

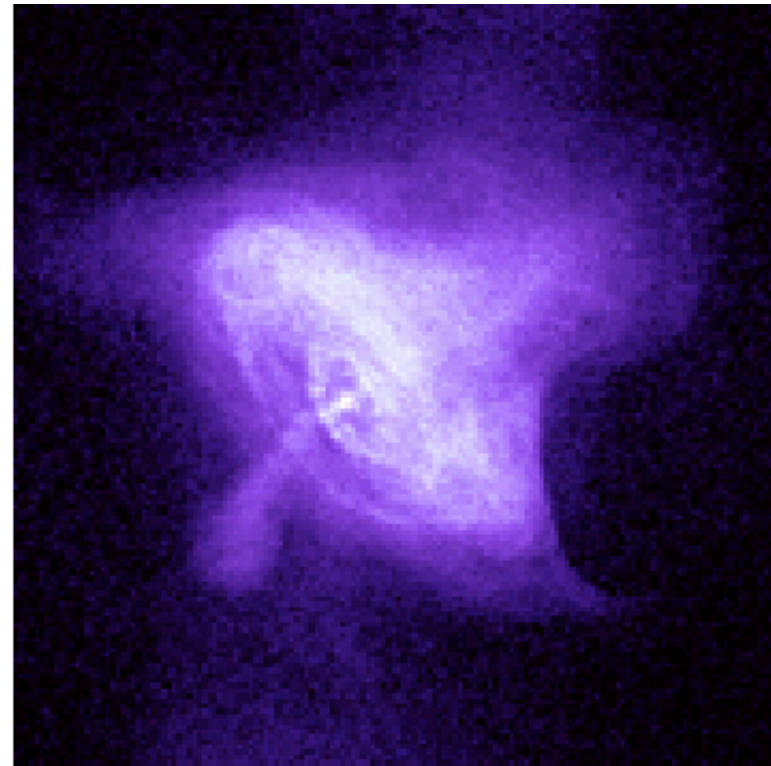
- *Focal length = 10 m*
- *1 module, 4 shells*
- *Coating = Iridium*
- *Angular Resolution = 0.5 arcsec HPD*



# *Chandra: a fantastic angular resolution*

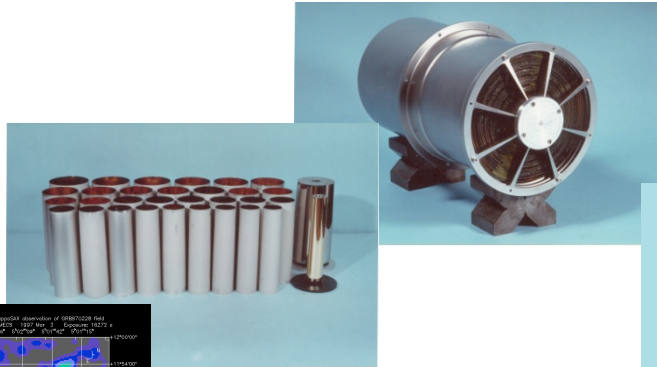


**Rosat: HPD = 3 arcsec**

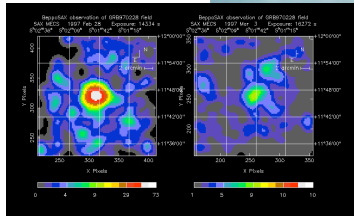


**Chandra: HPD = 0.5 arcsec**

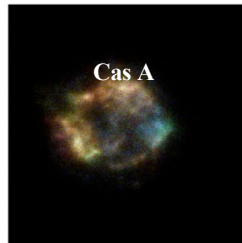
# X-ray optics by Ni electroforming replication



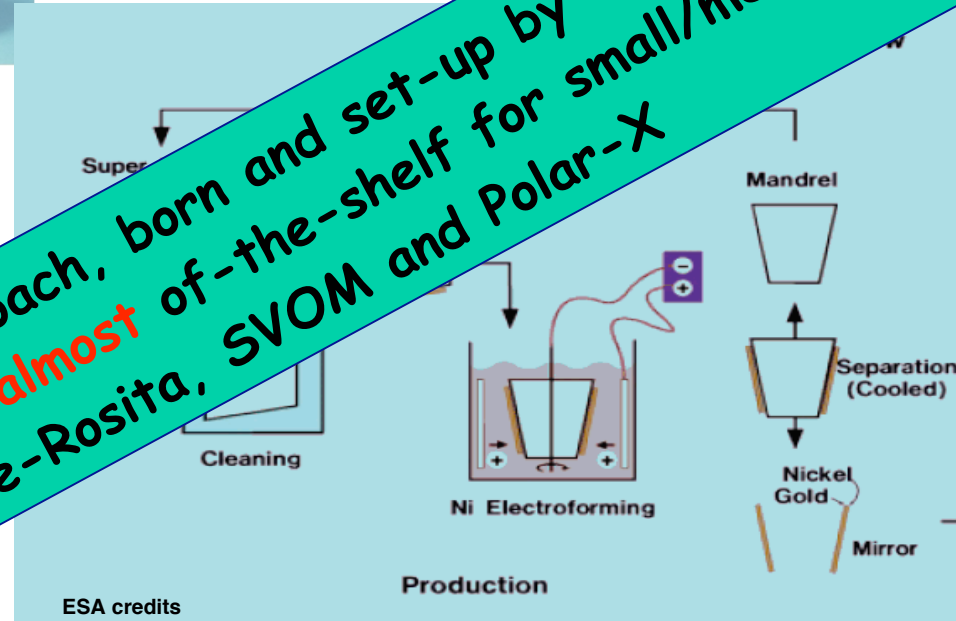
BeppoSAX



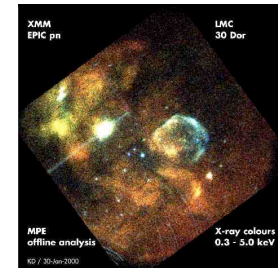
Jet-X/Swift



Cas A



Now the Ni electroforming approach, born and set-up by Citterio et al. For BeppoSAX is a technology **almost** of-the-shelf for small/medium size missions. It will be used for e-Rosita, SVOM and Polar-X

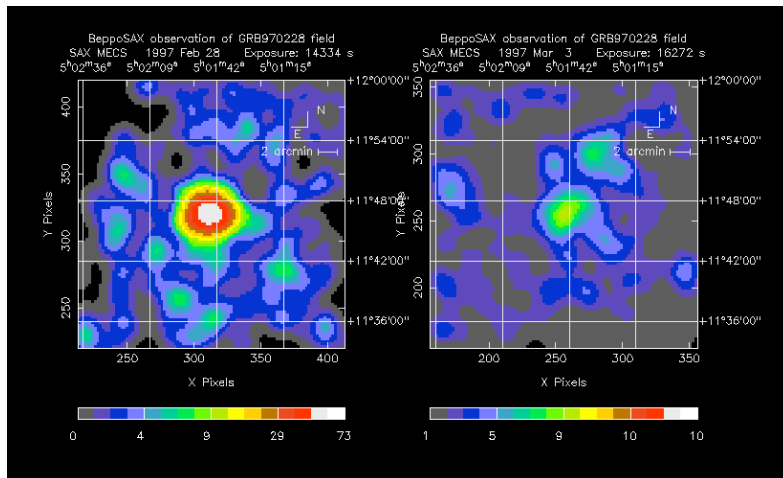
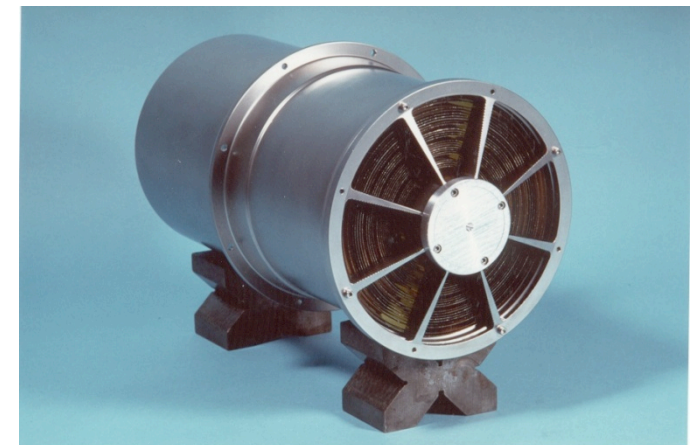
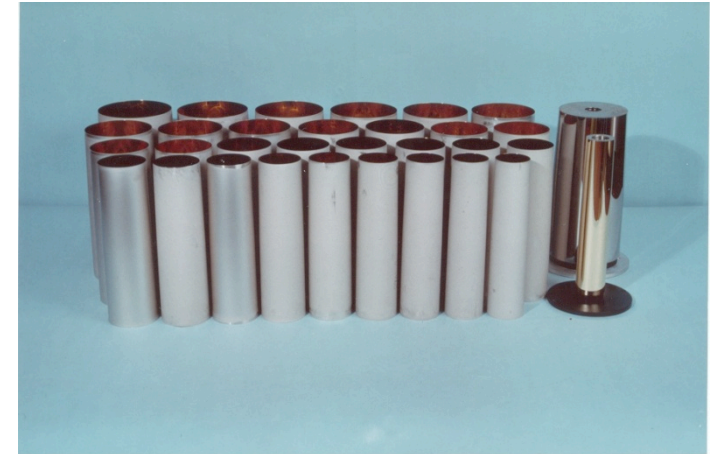


XMM-Newton



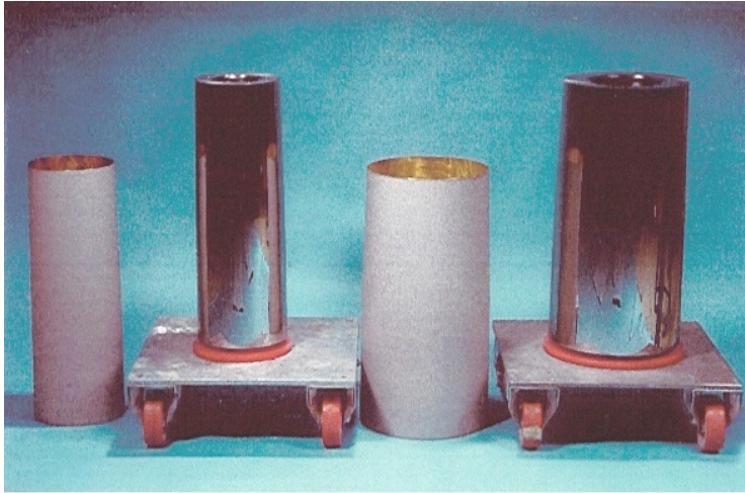
## Beppo-SAX soft X-ray (0.1 - 10 keV) concentrators

- Wolter I double-cone approx. - Au coating
- 4 modules - 30 shells/mod.
- F.L. = 180 cm Max diam = 16.1 cm
- $A_{eff}$  @ 1 keV = 85 cm<sup>2</sup> /module
- HEW= 60 arcsec (corresponding to the two-cones geom. aberration!)



GRB970228

## JET-X (optics ready since 1996) / SwiftXRT(2004) optics



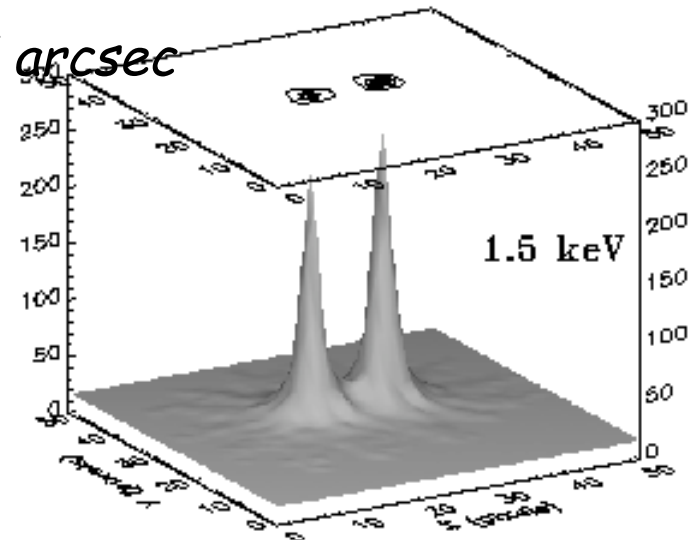
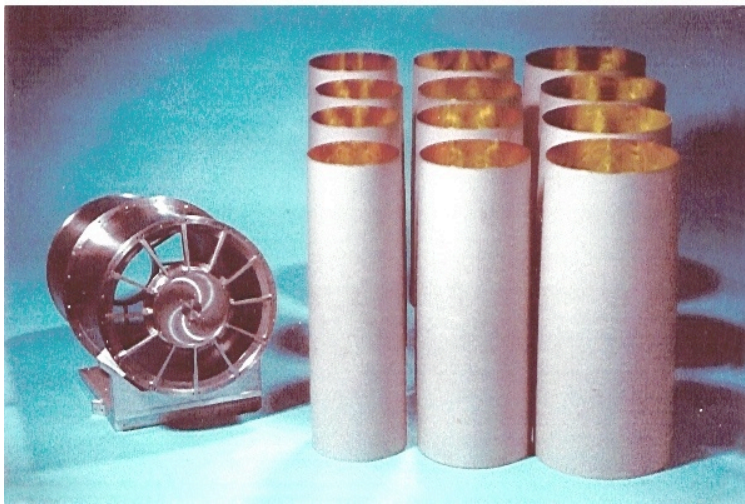
- Wolter I profile - Au coating (pathfinder of XMM)

- 2 mod. (JET-X) / 1 mod (Swift) - 12 shells/mod.

- F.L. = 350 cm - Max diam = 30 cm

- $A_{eff}$  @ 1 keV = 150 cm<sup>2</sup> /module

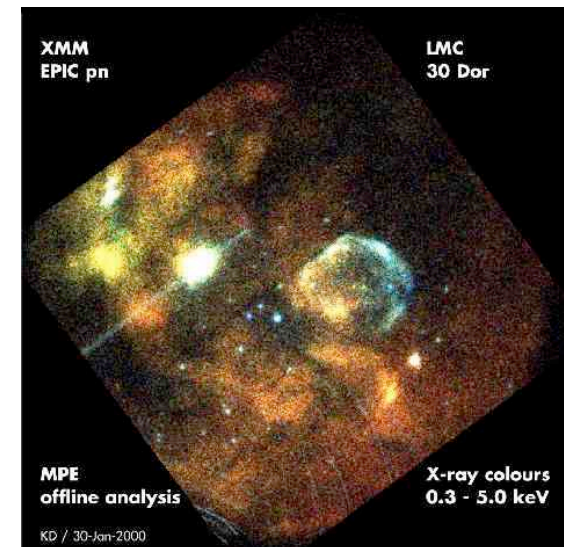
- HEW = 15 arcsec



Source separation: 20''

# *XMM-Newton (operational since dec. 1999)*

- *Wolter I profile - Au coating*
- *3 mod. - 58 shells/mod.*
- *F.L. = 750 cm - Max diam = 70 cm*
- $A_{eff} @ 1 \text{ keV} = 1500 \text{ cm}^2 / \text{module}$
- $HEW = 15 \text{ arcsec}$

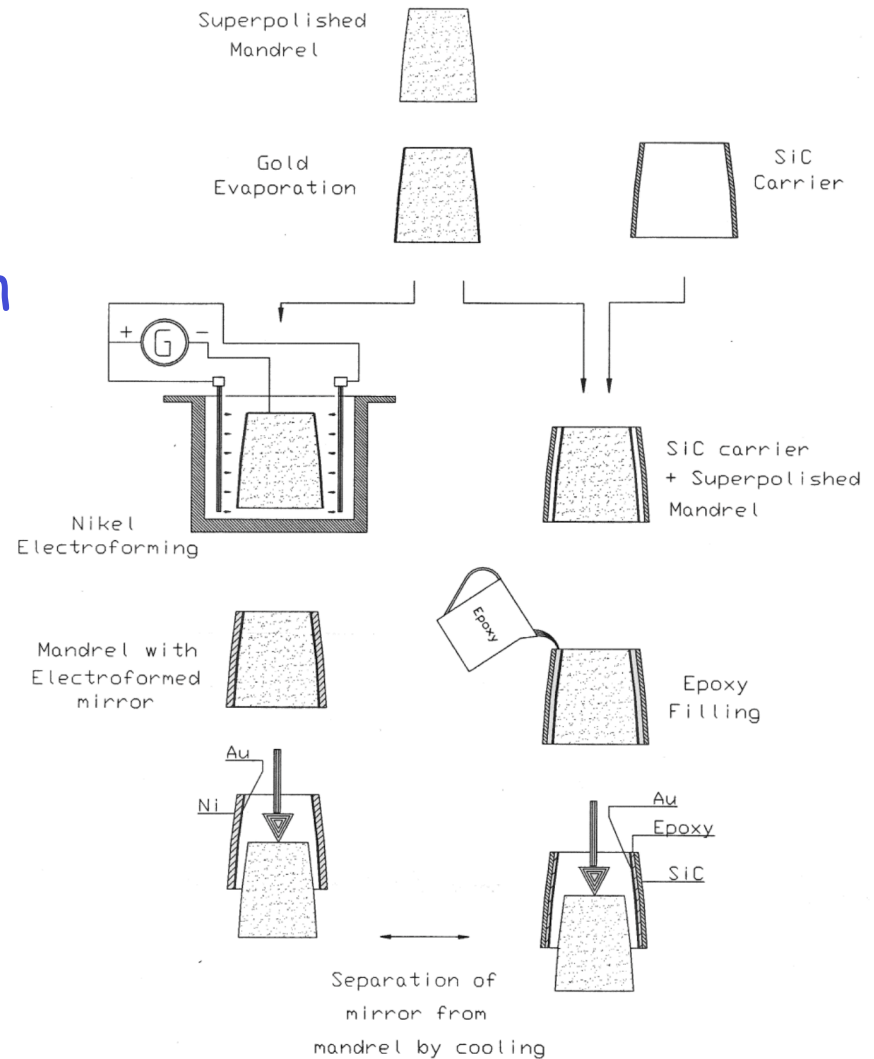


Credits: ESA

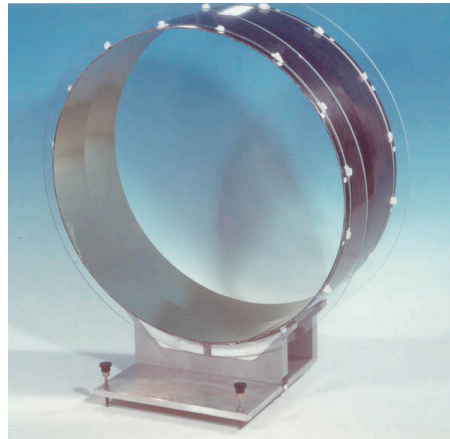
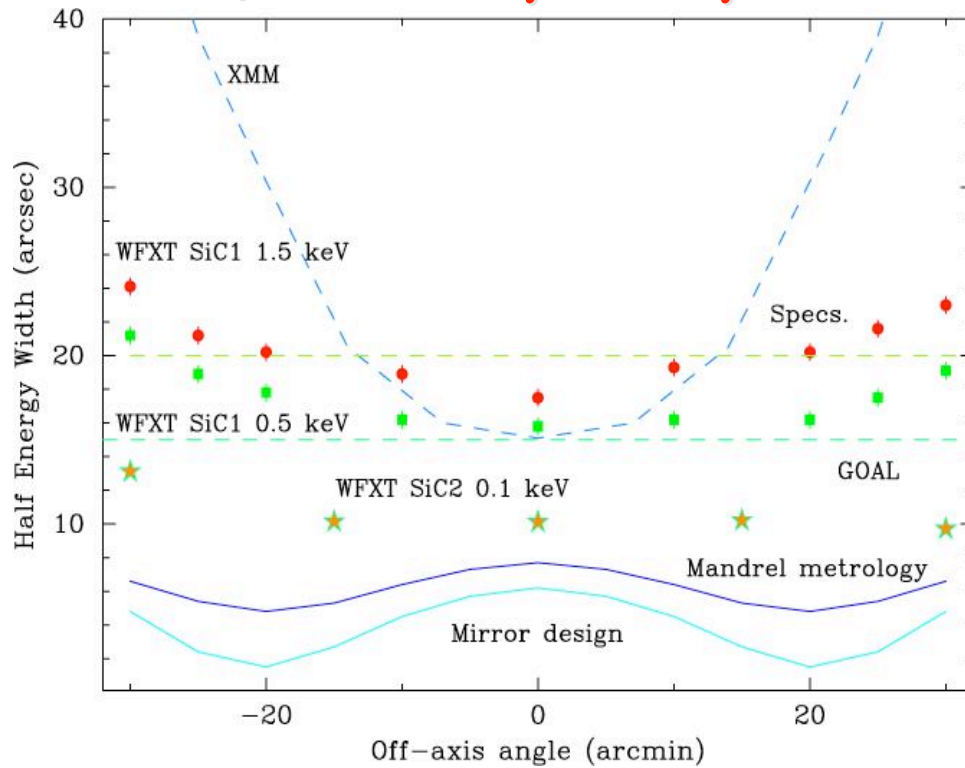
# Replication methods

- Ni electroforming replication (SAX, JET-X/Swift, XMM, ABRIXAS, e-ROSITA, SIMBOL-X, SVOM/XIAO)

- epoxy replication: EXOSAT (Be), WFXT (Alumina & SiC prototypes), EDGE/XENIA?



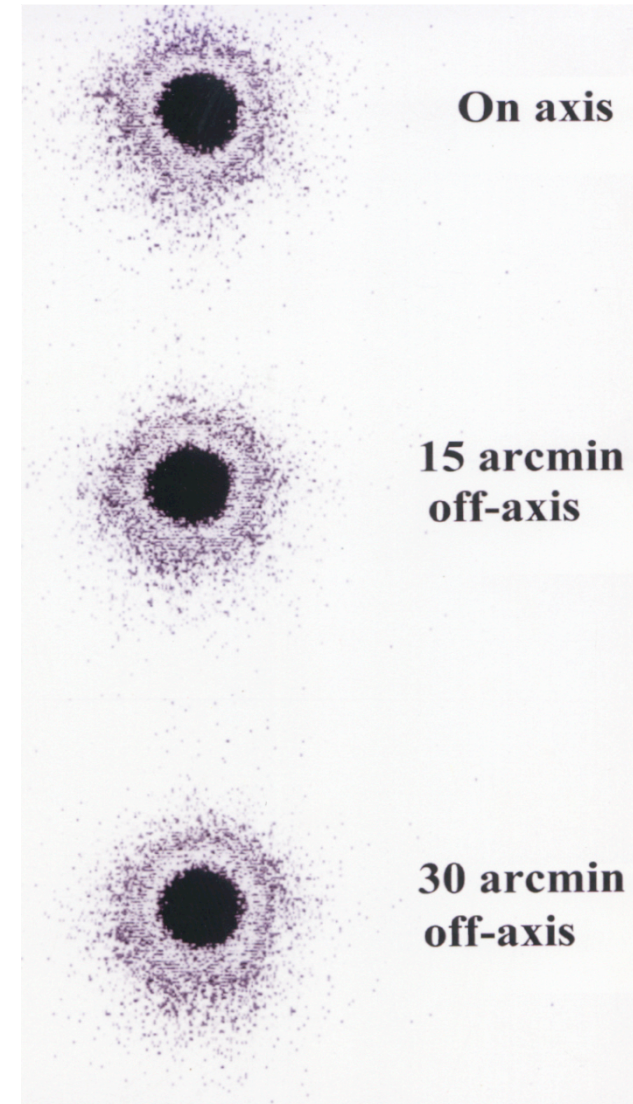
# WFXT (feasibility study 1997-1998) - Polynomial mirrors



WFXT (epoxy replication su carrier in SiC) -  $\varnothing = 60$  cm

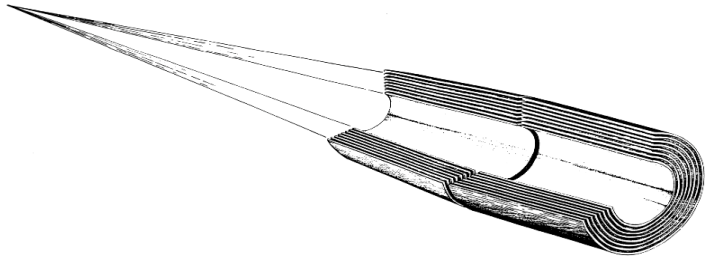
F. L. = 300 cm

*HEW = 10 arcsec*



Test @ Panter-MPE

# The focusing problem in the hard X-ray region (> 10 keV)



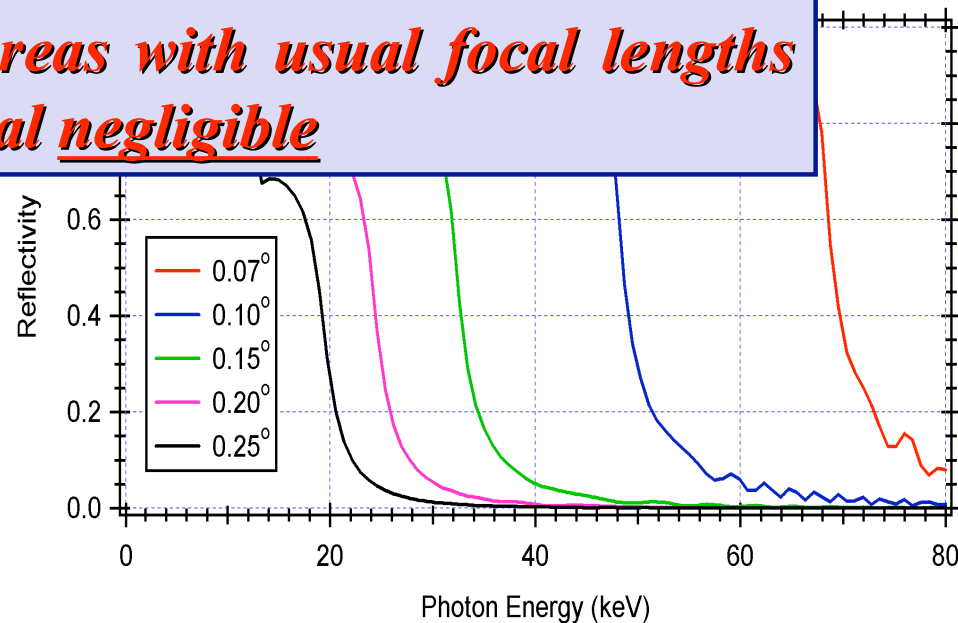
$$A_{\text{eff}} \approx F^2 \times \theta_c^2 \times R^2$$

At photon energies > 10 keV the cut-off angles for total reflection are very small also for heavy metals

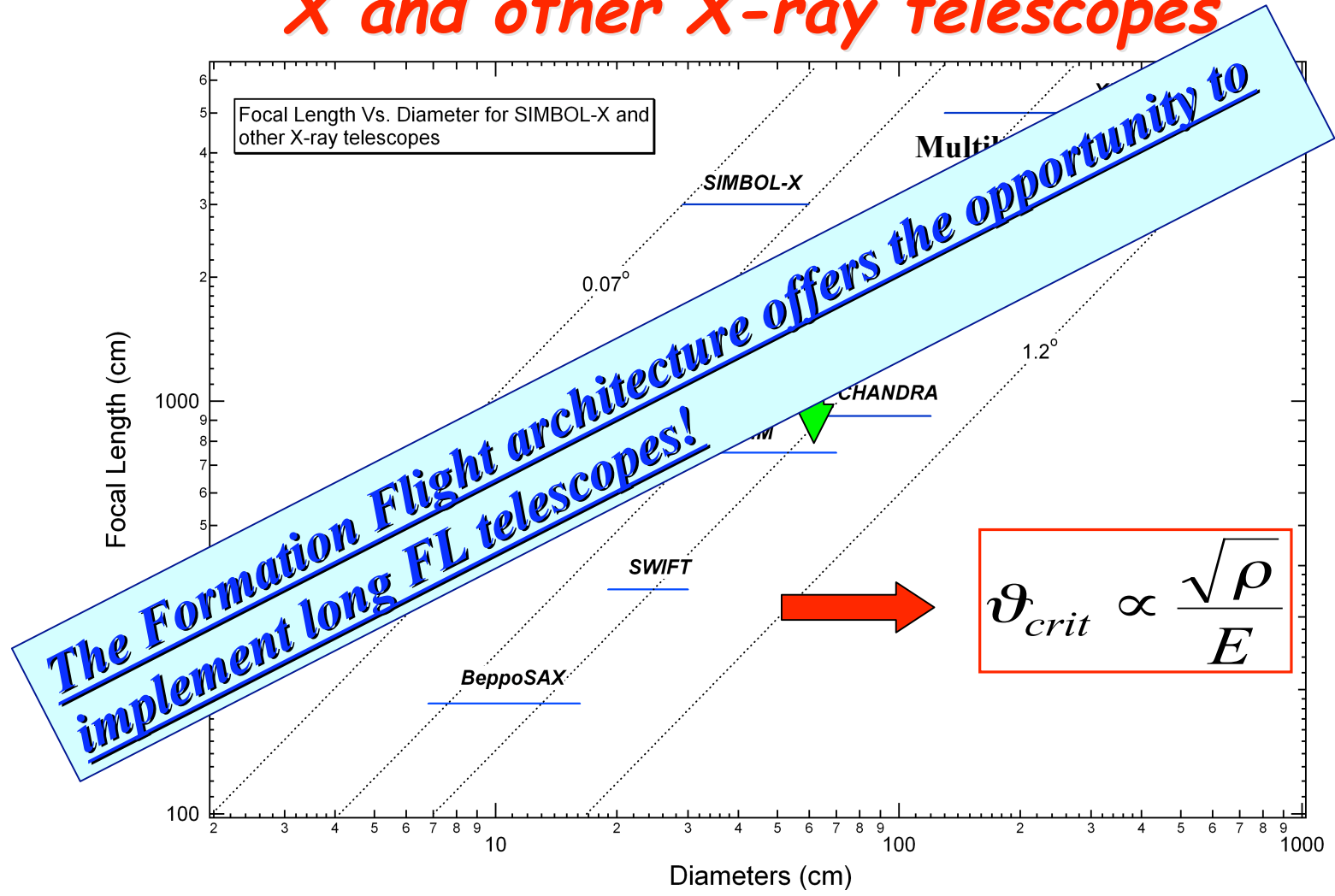
→ the geometrical areas with usual focal lengths (> 10 m) are in general negligible

but →

$$\vartheta_{\text{crit}} \propto \frac{\sqrt{\rho}}{E}$$

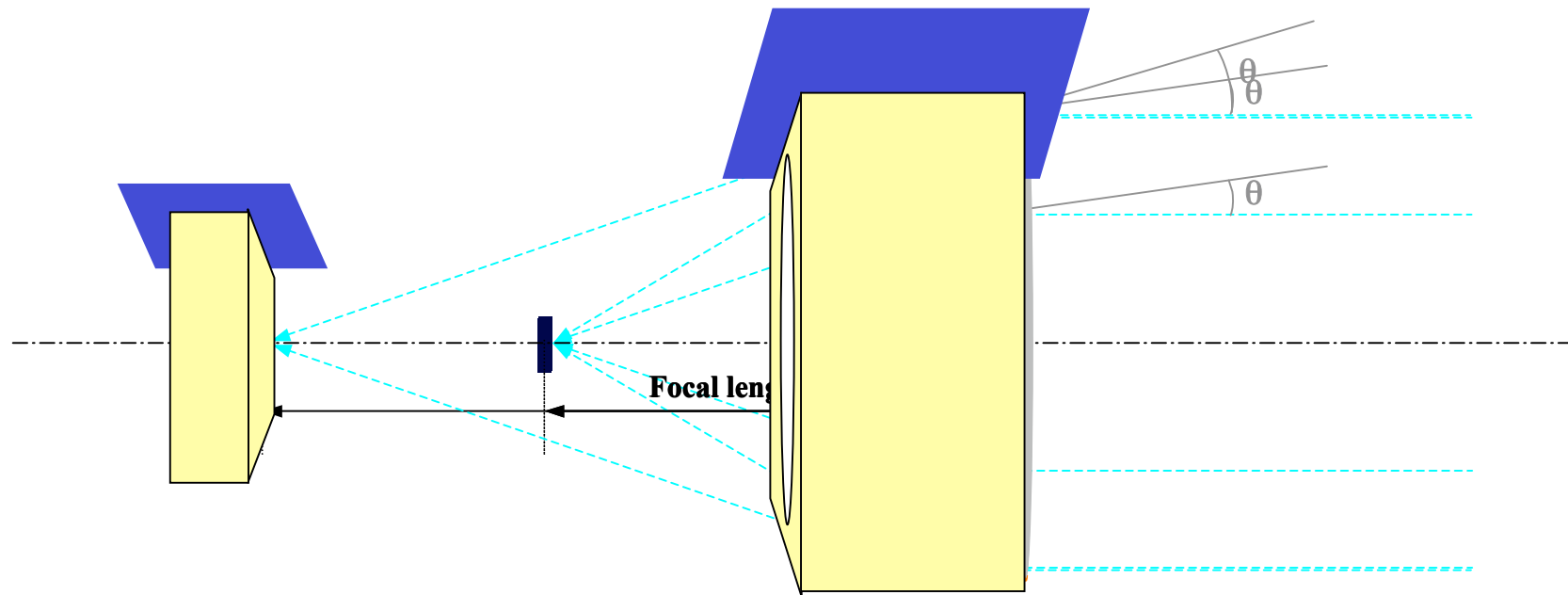


# Focal Length Vs. Diameters for SIMBOL-X and other X-ray telescopes



$$A_{eff} \approx F^2 \times \theta_c^2 \times R^2$$

# *The formation flight contribution*

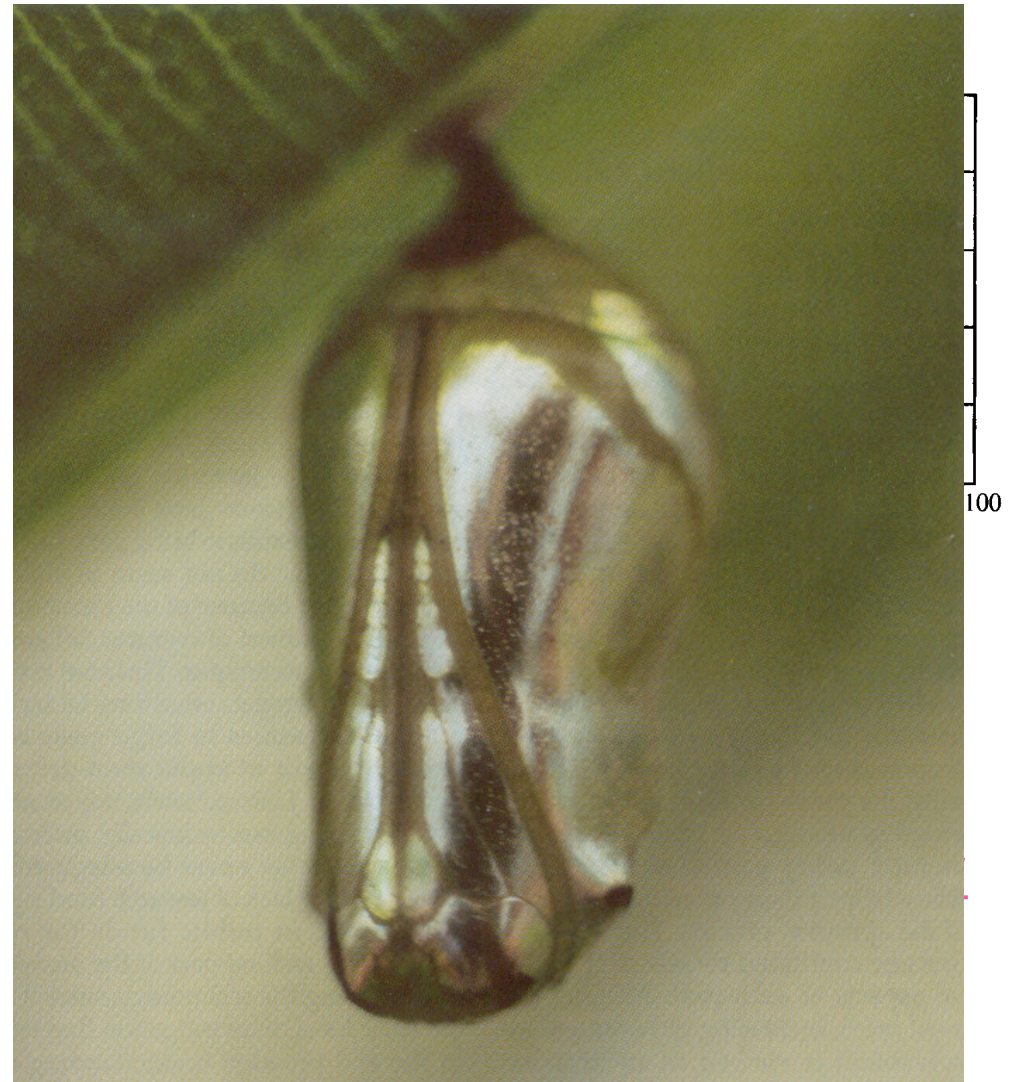
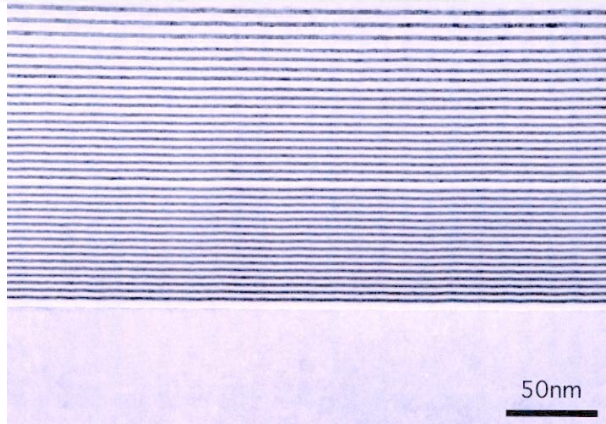
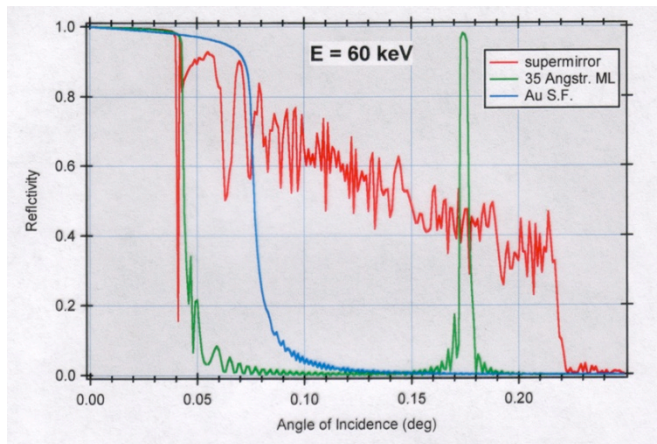




# Wide band multilayers

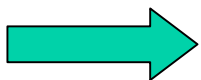
Optical supermirrors in a beetle skin

X-ray supermirrors



# Top-level scientific requirements

<i>Energy band:</i>	$\sim 0.5 - \geq 80$ keV
<i>Field of view (at 30 keV):</i>	$\geq 12'$ (diameter)
<i>On-axis effective area:</i>	$\geq 100$ cm <sup>2</sup> at 0.5 keV $\geq 1000$ cm <sup>2</sup> at 2 keV $\geq 600$ cm <sup>2</sup> at 8 keV $\geq 300$ cm <sup>2</sup> at 30 keV $\geq 100$ cm <sup>2</sup> at 70 keV $\geq 50$ cm <sup>2</sup> at 80 keV (goal)
<i>Detectors background</i>	$< 2 \times 10^{-4}$ cts s <sup>-1</sup> cm <sup>-2</sup> keV <sup>-1</sup> HED $< 3 \times 10^{-4}$ cts s <sup>-1</sup> cm <sup>-2</sup> keV <sup>-1</sup> LED
<i>On-axis sensitivity</i>	$\leq 10^{-14}$ c.g.s. ( $\sim 0.5$ $\mu$ Crab), 10-40 keV band, 3 $\sigma$ , 1Ms,
<i>Line sensitivity at 68 keV</i>	$< 3 \times 10^{-7}$ ph cm <sup>-2</sup> s <sup>-1</sup> (3 $\sigma$ , 1Ms)
<i>Angular resolution</i>	$\leq 20''$ (HPD), E < 30 keV $\leq 40''$ (HPD) @ E = 60 keV (goal)
<i>Spectral resolution</i>	$E/\Delta E = 40-50$ at 6-10 keV $E/\Delta E = 50$ at 68 keV (goal)
<i>Absolute timing accuracy</i>	100 $\mu$ s (50 $\mu$ s goal)
<i>Absolute pointing reconstruction</i>	$\sim 3''$ (radius, 90%) (2'' goal)
<i>Mission duration</i>	3 years including commissioning and calibrations (2 years of scientific program) + provision for a possible 2 year extension
<i>Total number of pointings</i>	$> 1000$ (first 3 years, nominal mission) $500$ (during the possible 2 year mission extension)



## *Simbol-X Optical Design*

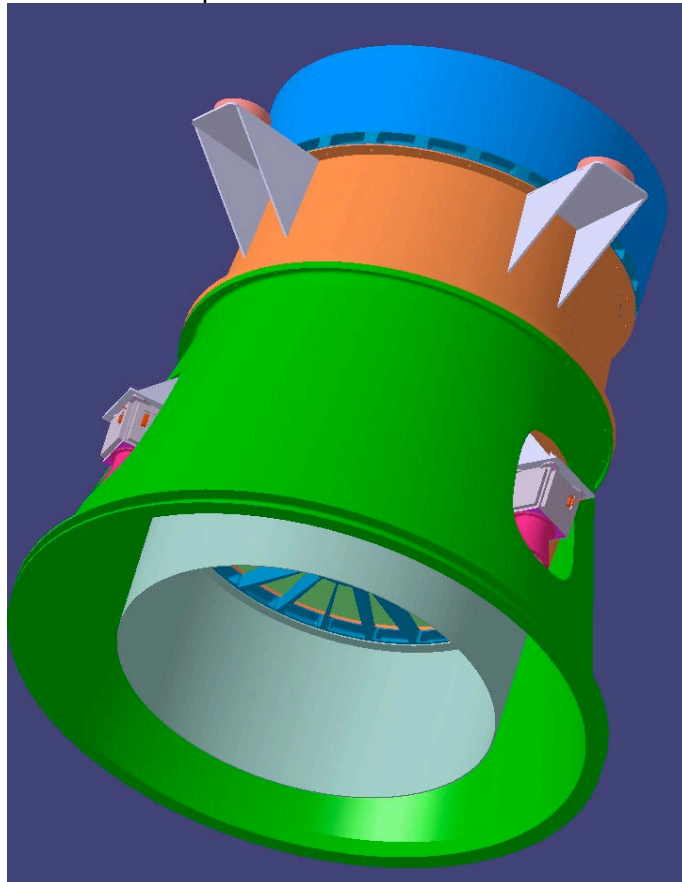
<b>Min-Max Diameter</b>	<b>250 - 650 mm</b>
<b>Focal Length</b>	<b>20000 mm</b>
<b>Mirror Height</b>	<b>600 mm</b>
<b>Configuration</b>	<b>Wolter I</b>
<b>Number of Mirror shells</b>	<b>100</b>
<b>Min-Max incidence angles</b>	<b>0.1° - 0.25°</b>
<b>Min-Max wall thickness</b>	<b>0.25 - 0.55 mm</b>
<b>Total Mirror Mass</b>	<b>287 kg</b>

**\_ NB: thickness trend 2 times less XMM-Newton**

# Symbol-X Optical Design

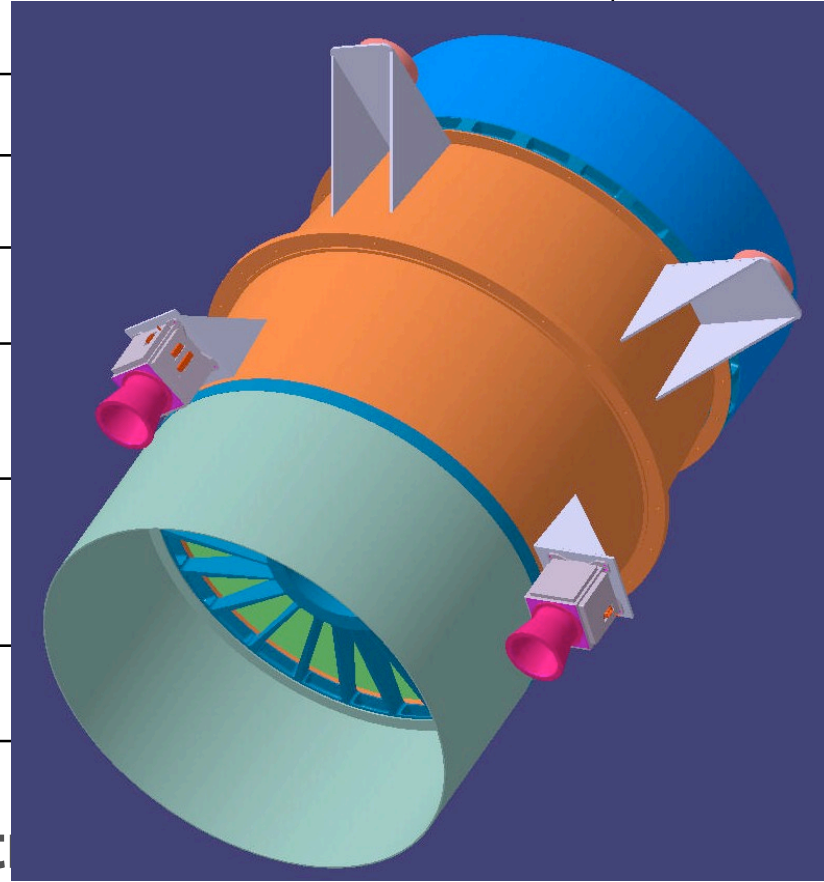
Min-Max Diameter

250 - 650 mm



Newton

ells

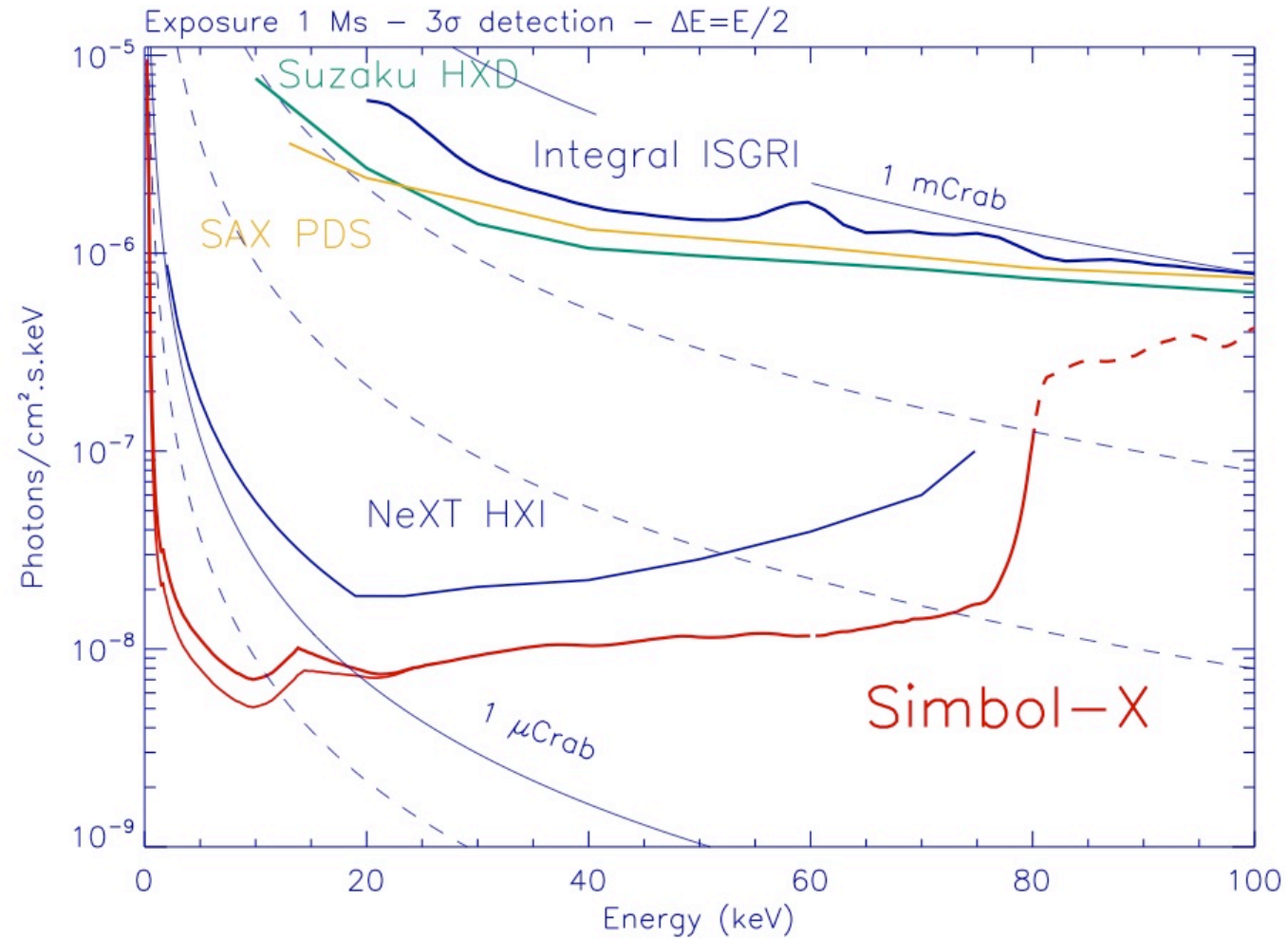


ess t

# *Angular resolution for past & future Hard X-ray Experiments*

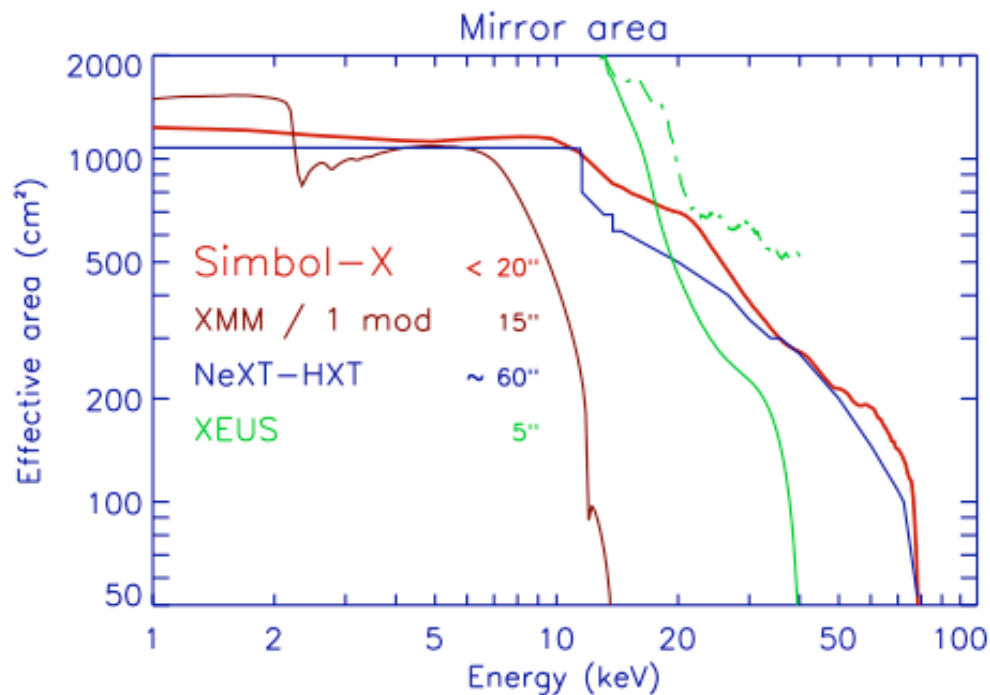
<i>Experiment</i>	<i>Year</i>	<i>"Imaging" technique</i>	<i>Angular resolution</i>
SAX-PDS	1996	Rocking collimator	> 3600 arcsec (collimator pitch)
INTEGRAL- IBIS	2002	Coded mask	720 arcsec (mask pitch)
HEFT (balloon)	2005	Multilayer optics	> 90 arcsec HEW
NUSTAR	2011	Multilayer Optics	40-60 arcsec HEW
<b><i>SIMBOL-X</i></b>	<b><i>2014</i></b>	<b><i>Multilayer Optics</i></b>	<b><i>15-20 arcsec HEW</i></b>

# Expected Flux Sensitivity



# Simbol-X Optics

- Heritage from XMM-Newton : nickel shells obtained by electroforming replication method; low mass obtained via a reduced thickness of shells
- Coating : multi-layer Pt/C needed for requirement on large FOV and on sensitivity up to > 80 keV

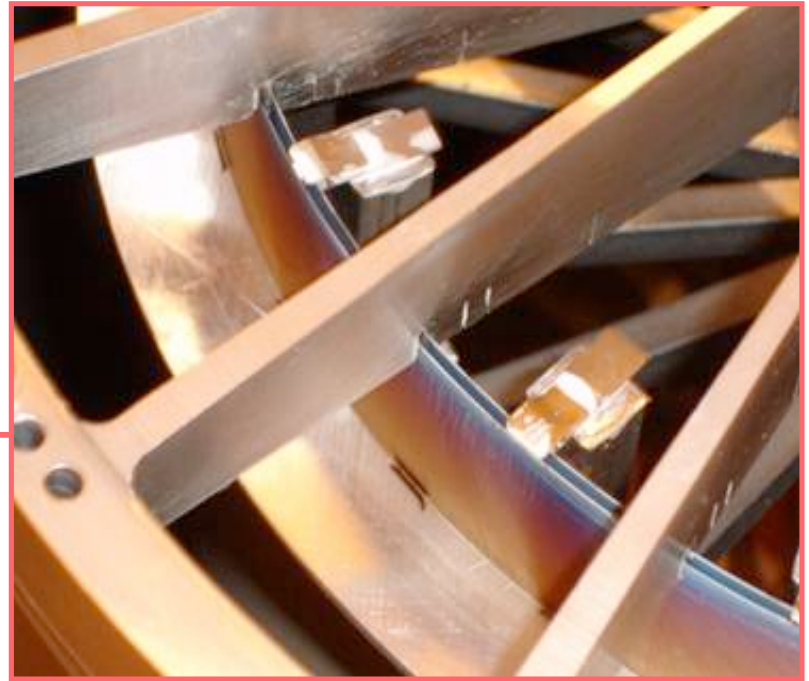


Focal length : 20 m  
Shell diameters : 30 to 70 cm  
Shell thickness : 0.2 to 0.6 mm  
Number of shells : 100

N.B. I: The optics module will have both sides covered with thermal blankets

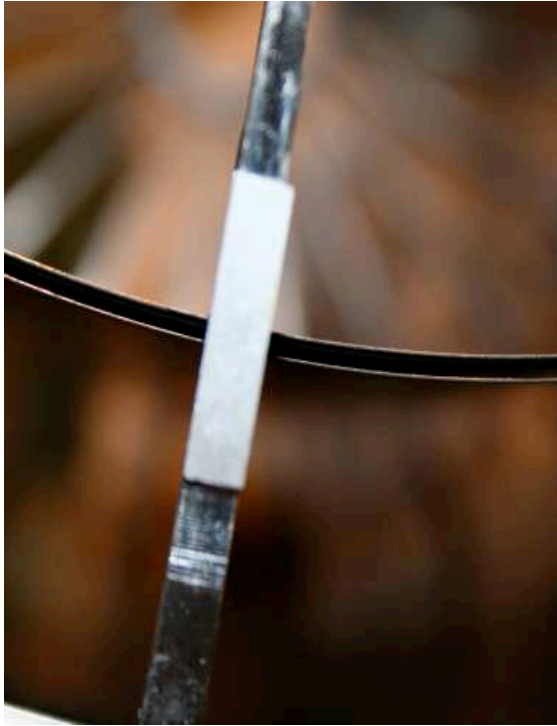
N.B. II: a proton diverter will be implemented

# *Integration of thin mirror shells*

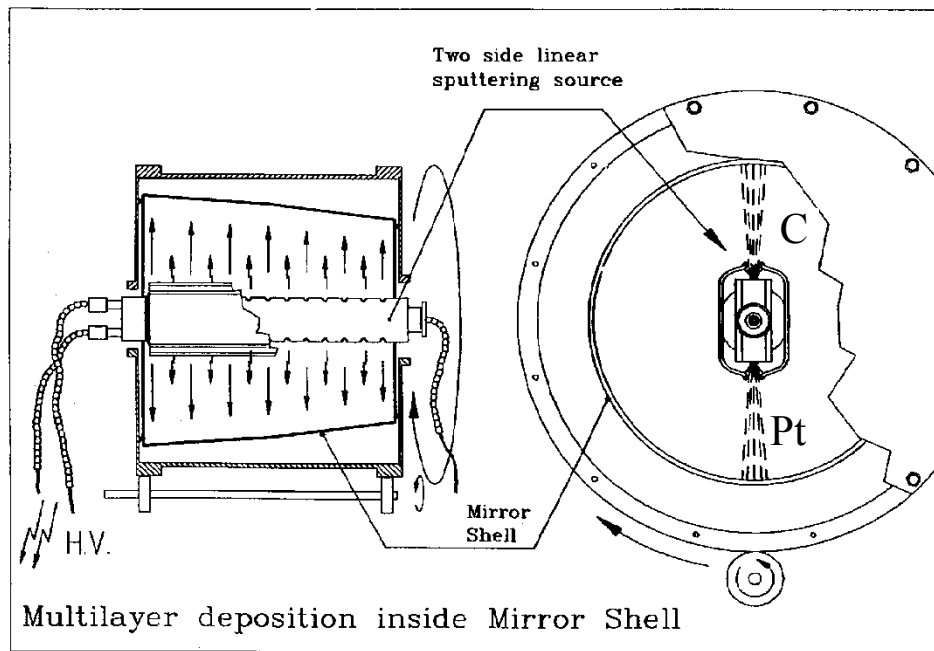




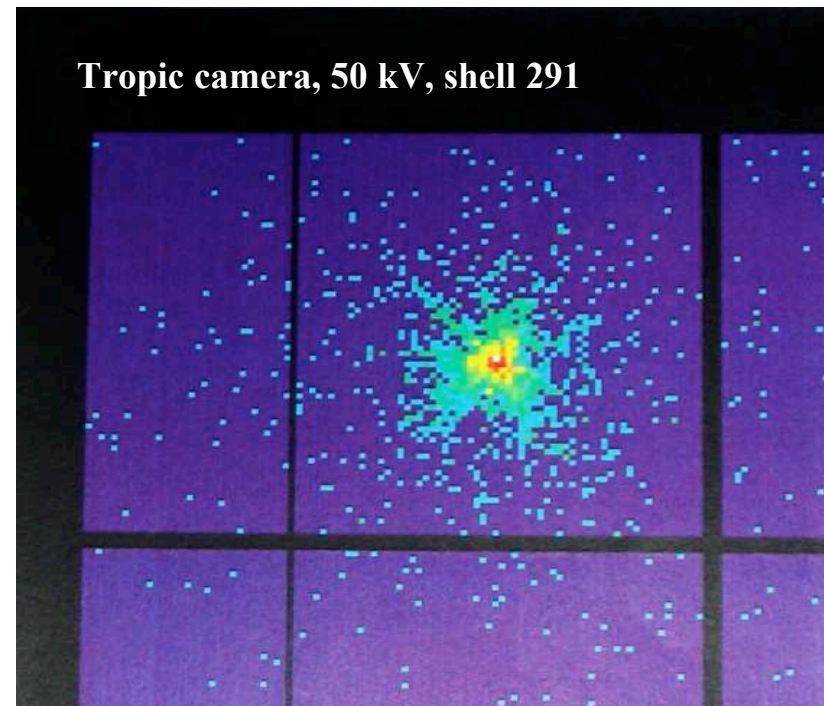
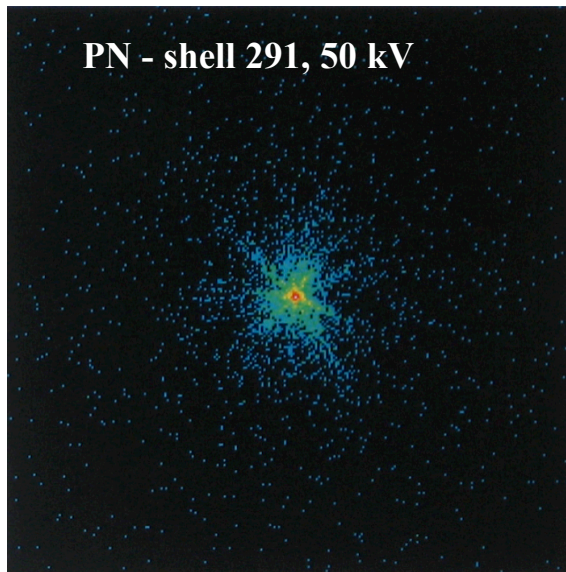
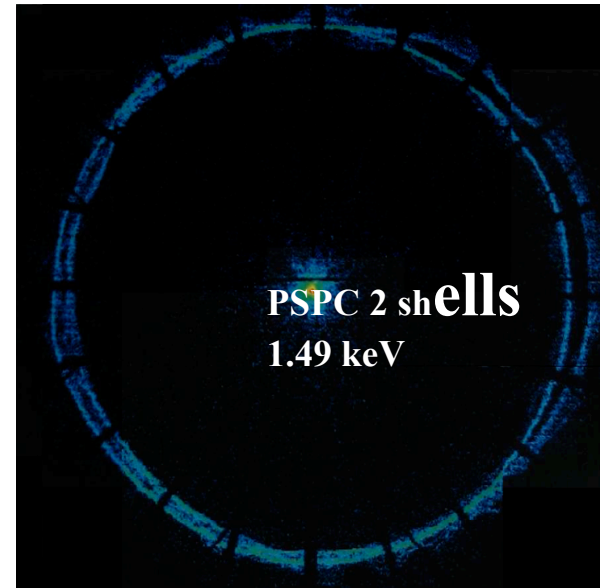
# *Integration of thin mirror shells*



# Multilayer deposition concept



*Calibration of the 2 mirror shell prototype at Panter MPE*

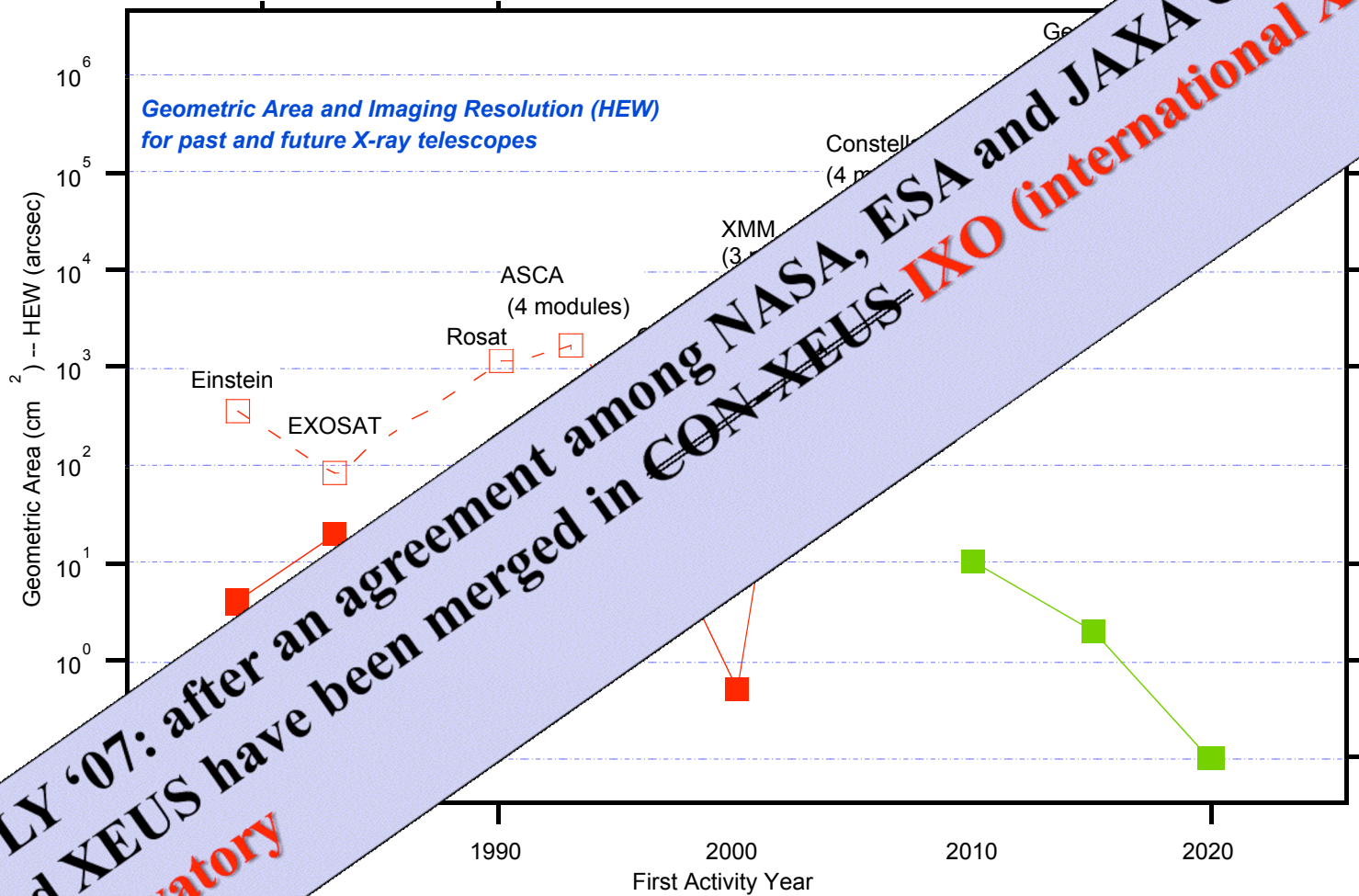


## *Calibration of 2 mirror shell prototype at Panter MPE*

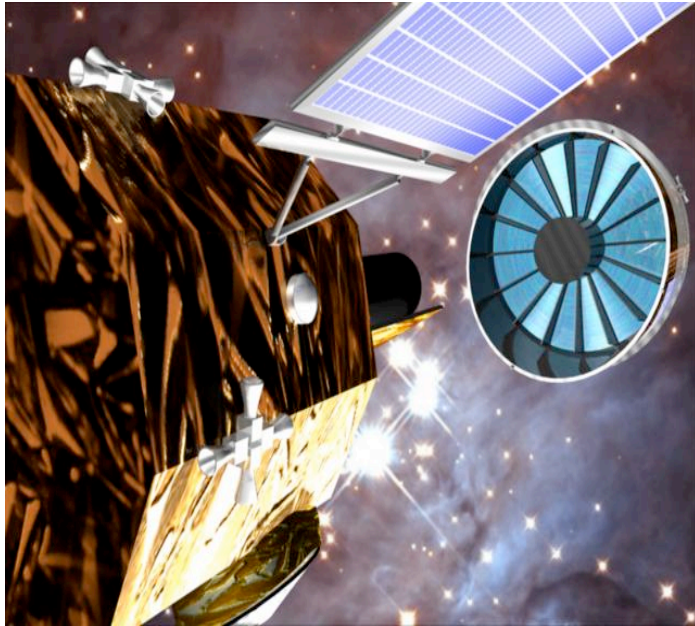
Energy (keV)	HEW (arcsec) 291 shell	HEW (arcsec) 295 shell
1.5	23	22.5
8	24	27.5
20	27	29
35	31	49
50	33	49



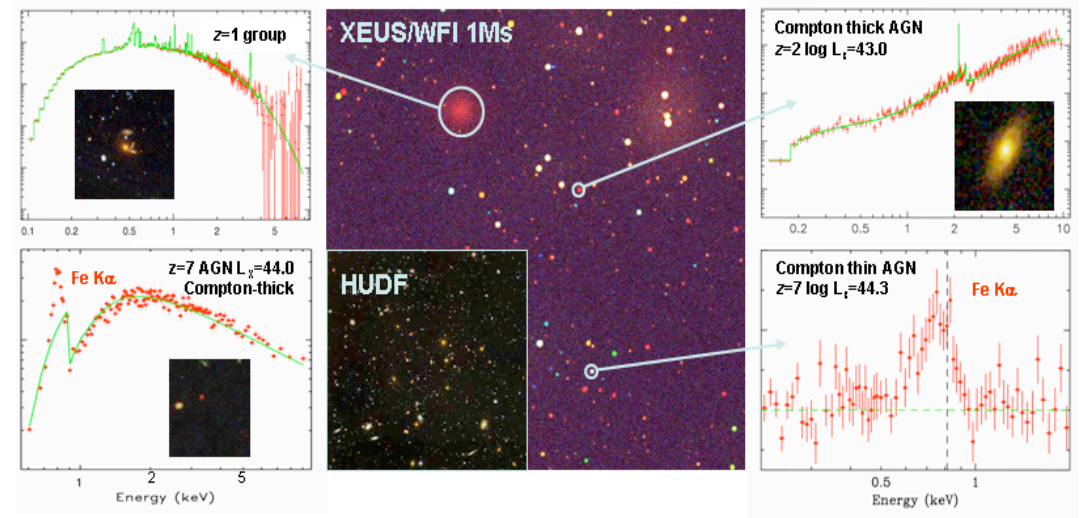
# Where are we going?



**JULY '07: after an agreement among NASA, ESA and JAXA Con-X and XEUS have been merged in CON-XEUS-IXO (international X-ray Observatory)**



# XEUS



**Sensitivity (cgs)**  $(3 \times 10^{-18})$  @ 0.2–8 keV; 4\_

## Effective Area

- 1 (1.5) m<sup>2</sup> @ 0.2 keV
- 5 m<sup>2</sup> @ 1 keV
- 2 m<sup>2</sup> @ 7 keV
- 1 m<sup>2</sup> @ 10 keV
- (0.1) m<sup>2</sup> @ 30 keV

## Angular Resolution

- 5 (2) arcsec @ < 10 keV
- 10 arcsec @ 40 keV

## Field-of-View

- 7 (10) arcmin diameter: WFI, HXI
- 1.7 arcmin diameter: NFI

## ***XEUS X-ray optics requirements***

<i><b>ITEM</b></i>	<i><b>Requirement</b></i>	<i><b>Goal</b></i>
<b>Angular Resolution (HFW)</b>	<b>5 arcsec</b>	<b>2 arcsec</b>
<b>Collecting Area @ 1 keV</b>	<b>5 m<sup>2</sup></b>	<b>5 m<sup>2</sup></b>
<b>Collecting Area @ 7 keV</b>	<b>2 m<sup>2</sup></b>	<b>2m<sup>2</sup></b>

N.B. data from the proposal document



## *Optics mass budget*

Mirrors	Support	ancillary	Total
882 kg	176 kg	238 kg	1296 kg

N.B. data from the proposal document

## *Optics error budget*

<i>Specification (arcsec)</i>	<i>Inherent</i>	<i>Intrinsic</i>	<i>Extrinsic</i>	<i>Environment</i>	<i>Total</i>
<b>Goal</b>	1.4	1.2	0.5	0.5	2
<b>Requirement</b>	1.8	3.7	2	2	5

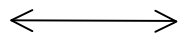
N.B. data from the proposal document

## *Optics Characteristics*

<i>Characteristic</i>	<i>Value</i>
<b>Pore size</b>	<b>0.6 × 1.5 mm<sup>2</sup></b>
<b>Aperture radii</b>	<b>0.67-2.1 m</b>
<b>Grazing reflection angles</b>	<b>0.27-0.86 degrees</b>
<b>Focal length</b>	<b>35 m</b>
<b>Plate scale</b>	<b>170_m/arcsec</b>

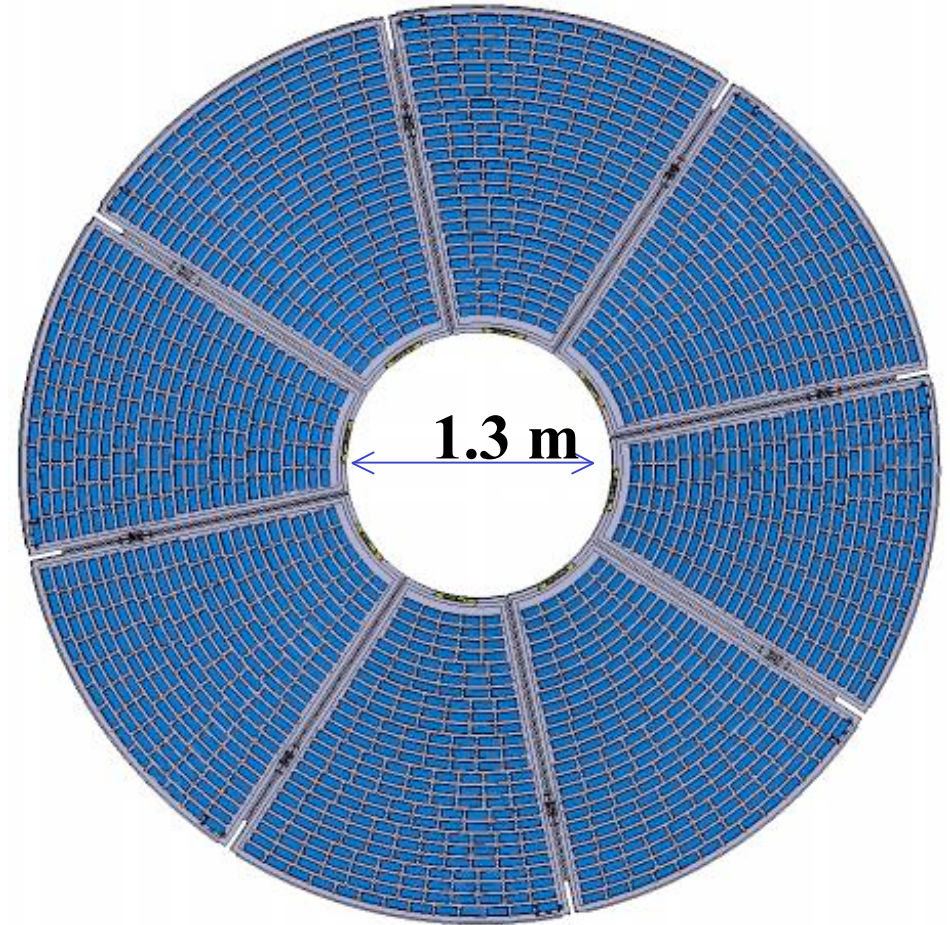
N.B. data from the proposal document

**XMM**

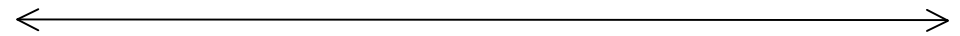


**0.7 m**

**XEUS**



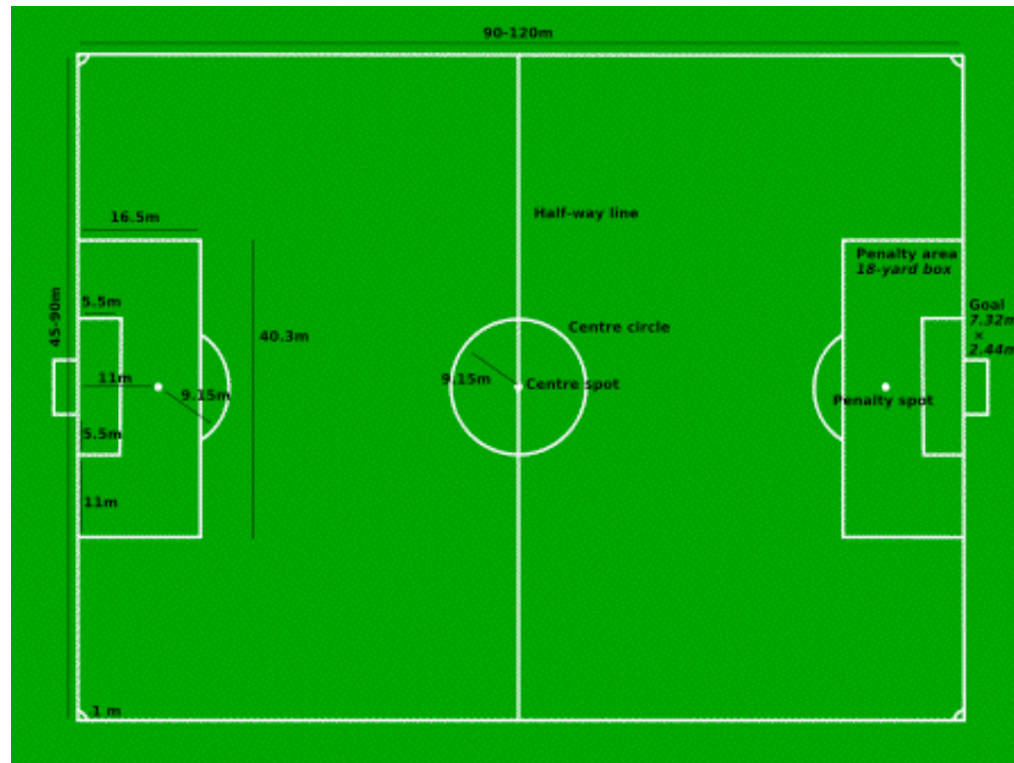
**1.3 m**



**4.5 m**

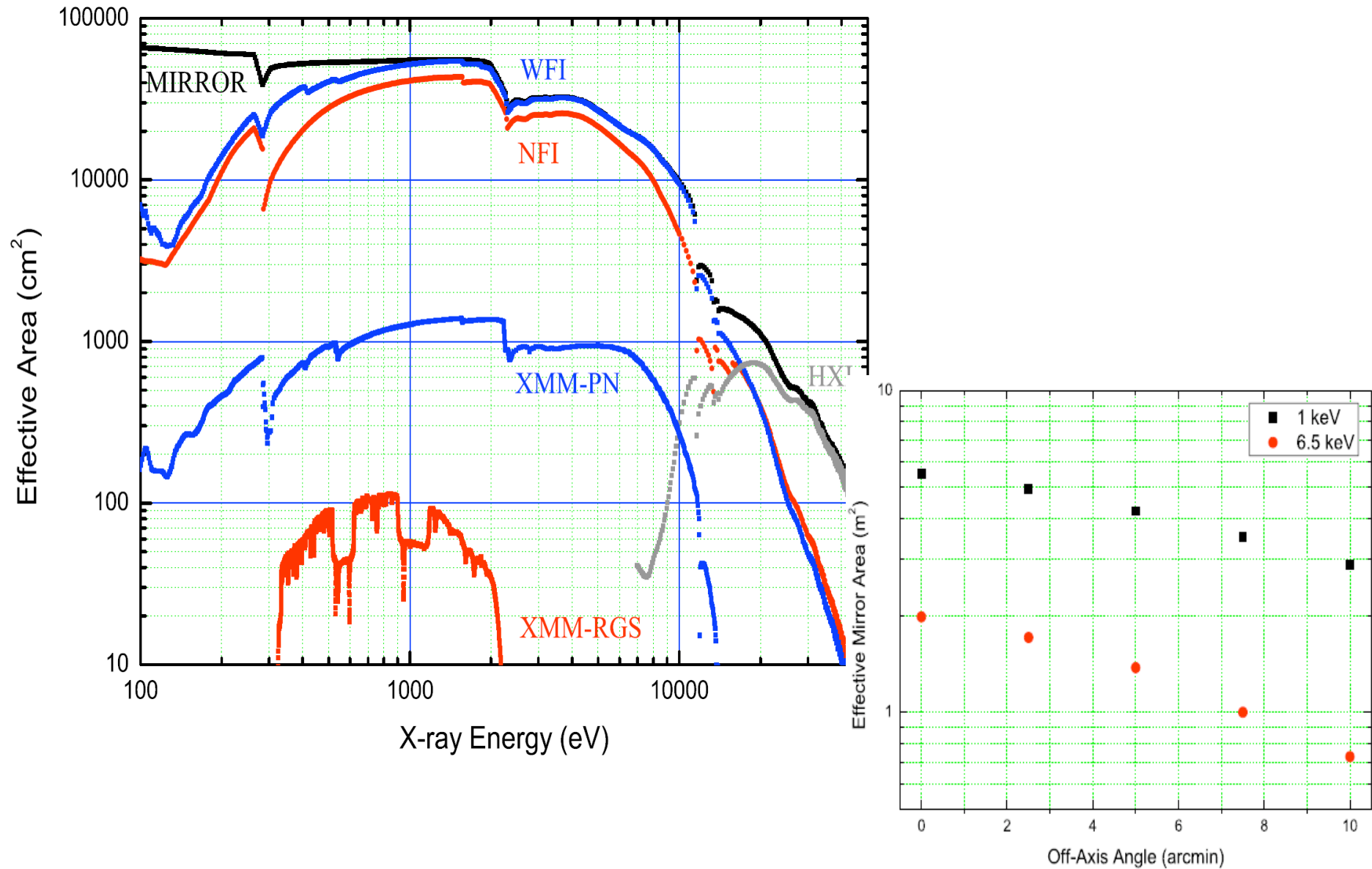
# *Total reflecting surface to be produced*

**2.5 x**



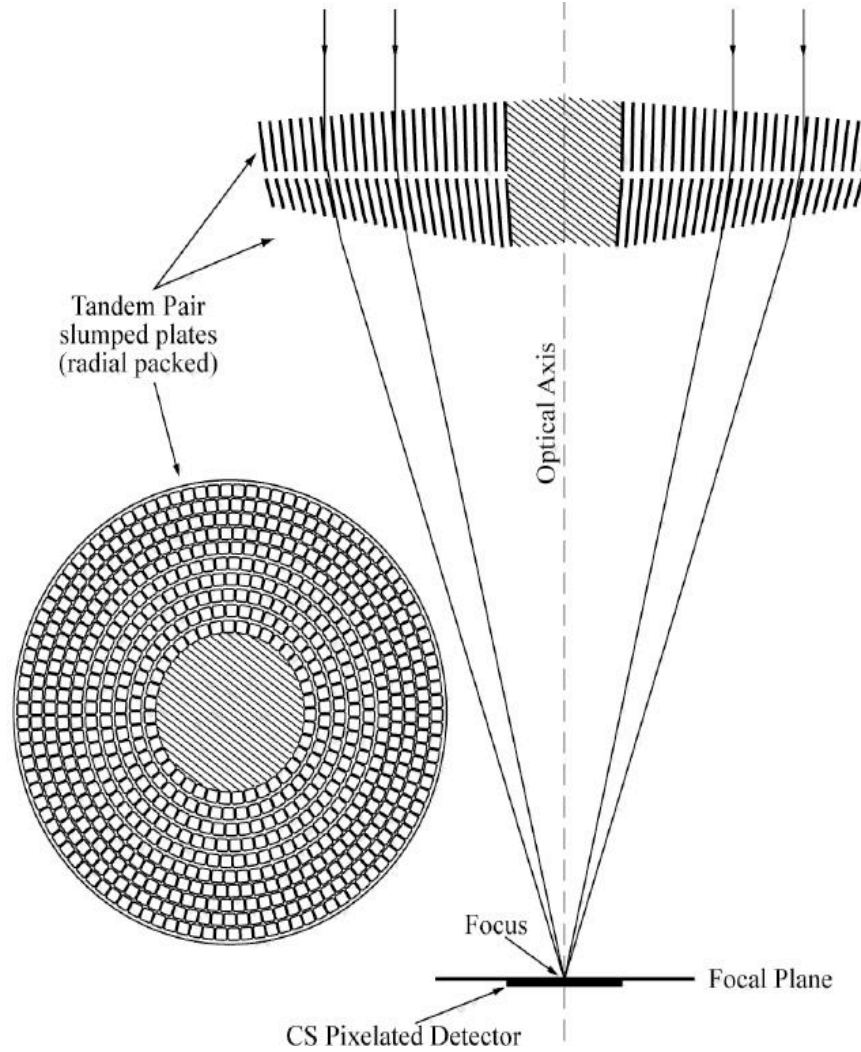
**Need of a manufacturing process scalable at a high volume production industrial level!**

# *XEUS Effective Area*



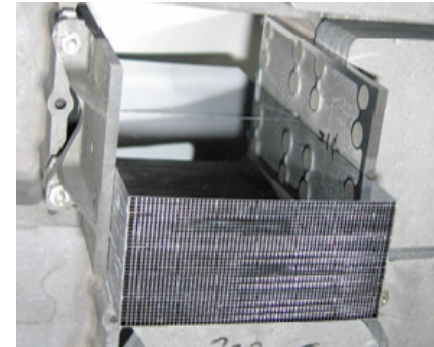
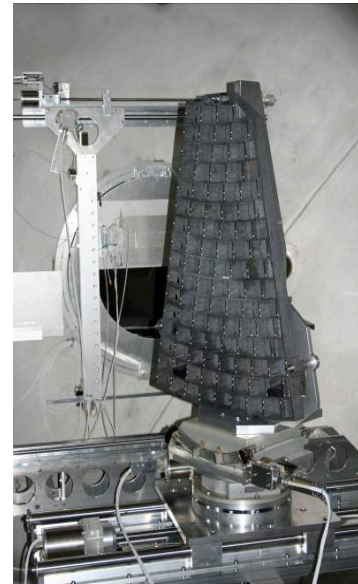
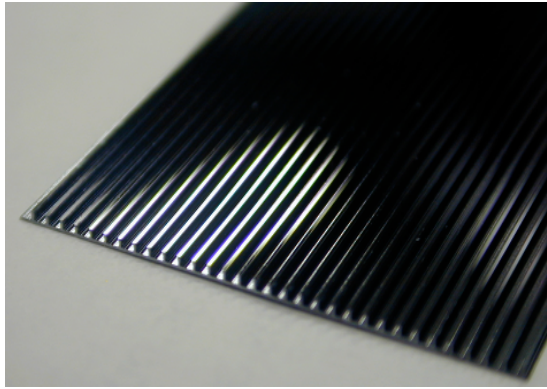
# X-ray Pore Optics System

## Double-Cone approximation



*N.B. :concept introduced by D. Willingale et al, Capri 1994*

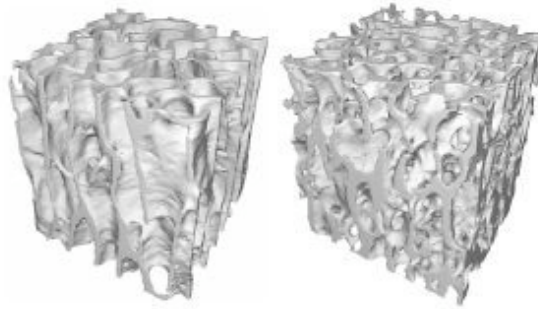
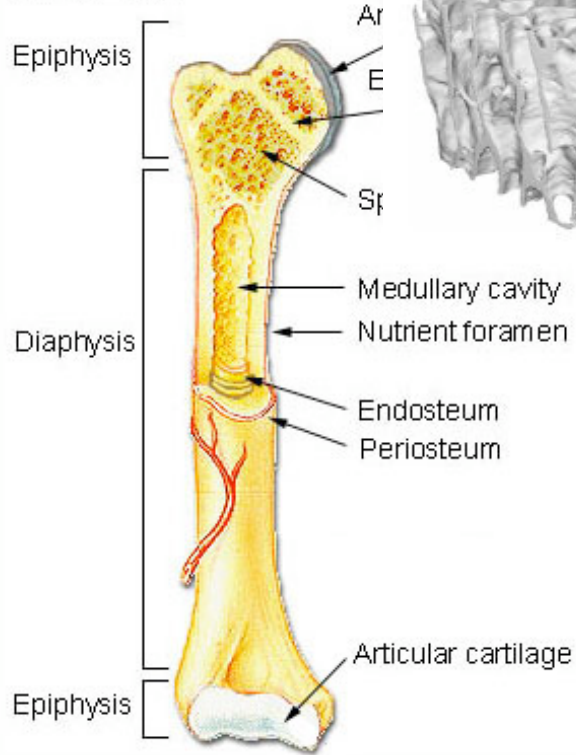
# *Pore Optics technology*



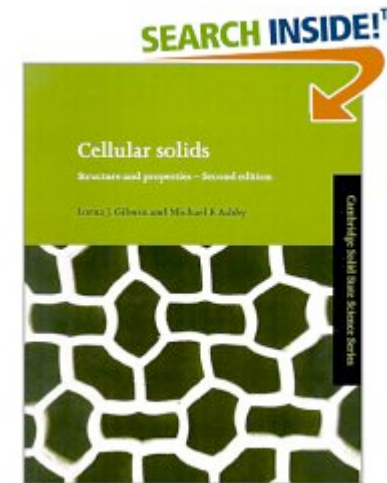
**Credits: ESA & Cosine**

# Cellular solids: light weight structures with a very high stiffness

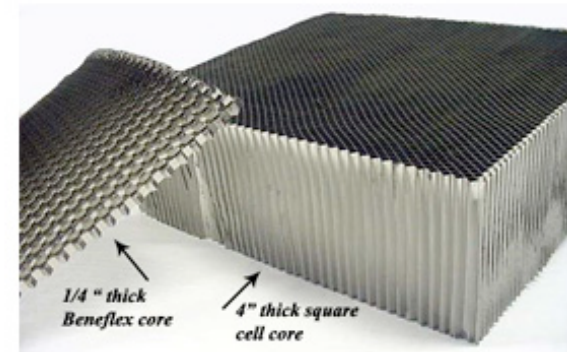
## Long Bone



**Foamed**

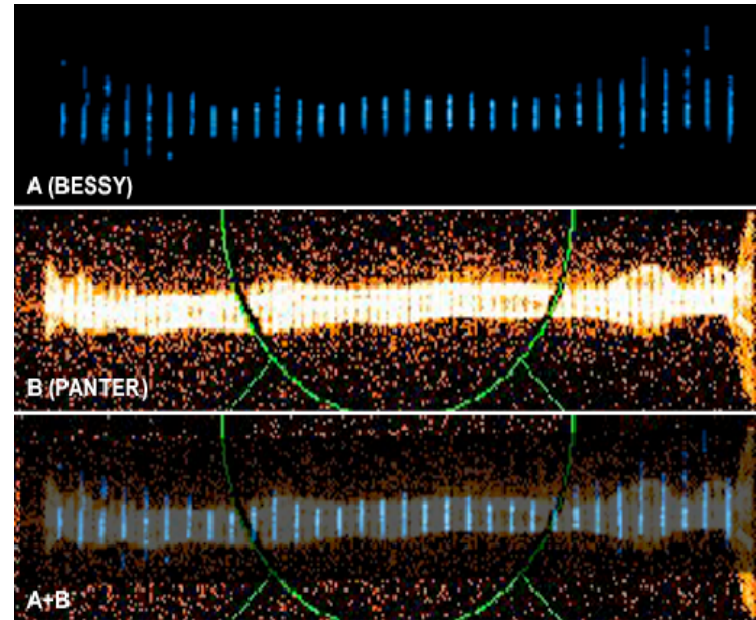
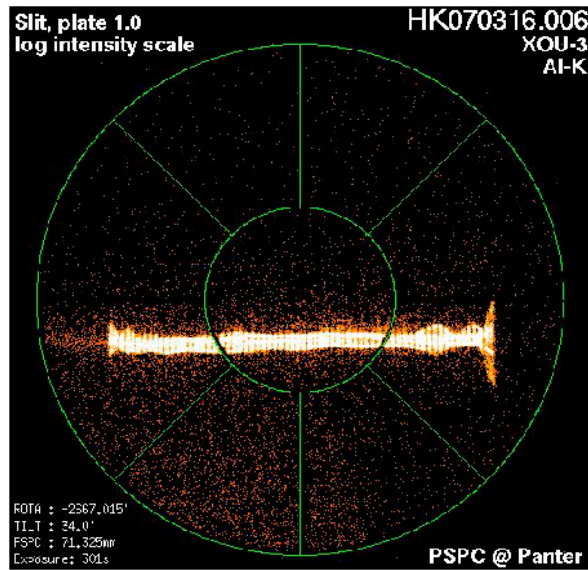


**Regular cellular structures**





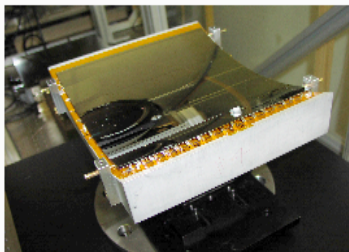
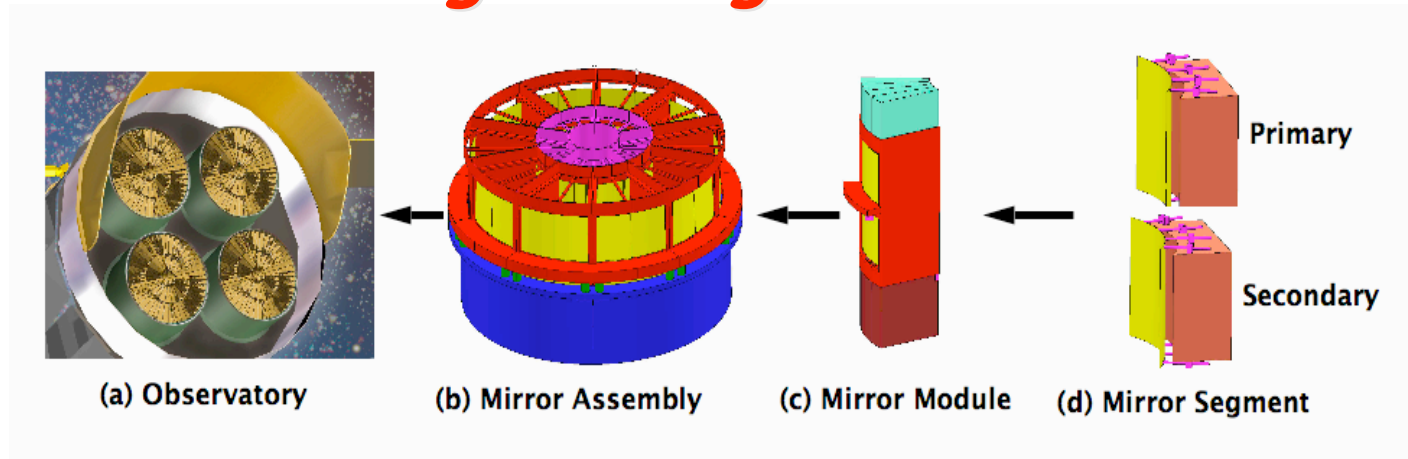
# *Preliminary imaging tests onto two-reflection optics (I)*



**Credits: ESA, Cosine, MPE**

**Collon et al, SPIE Proc 67898, in press (2007)**

# Alternative approach: hot sluping of thin glass segments



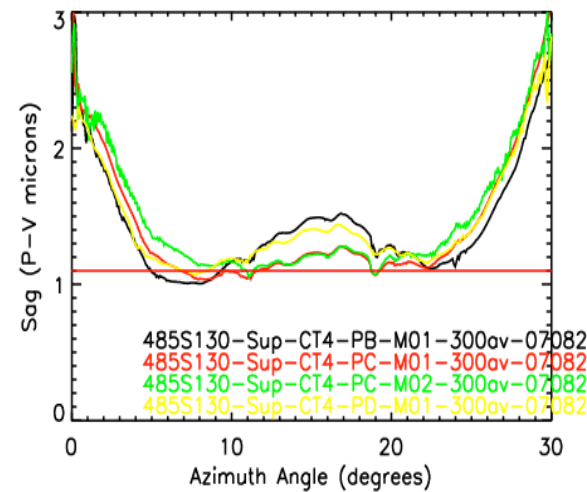
Mattress



Cantor Tree



Suspend & Bond

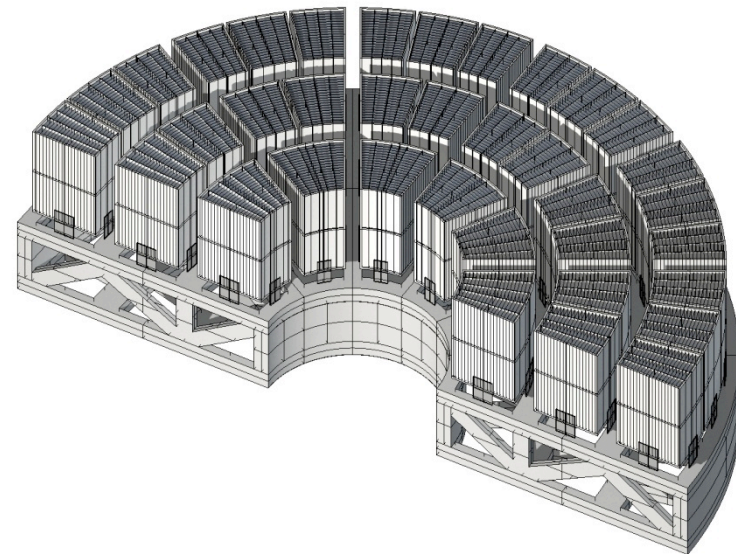


**0.4 mm thick segments 1 tandem (without integration)**  
**HEW = 13 arcsec**

## *Wolter I preliminary design for XEUS (I)*

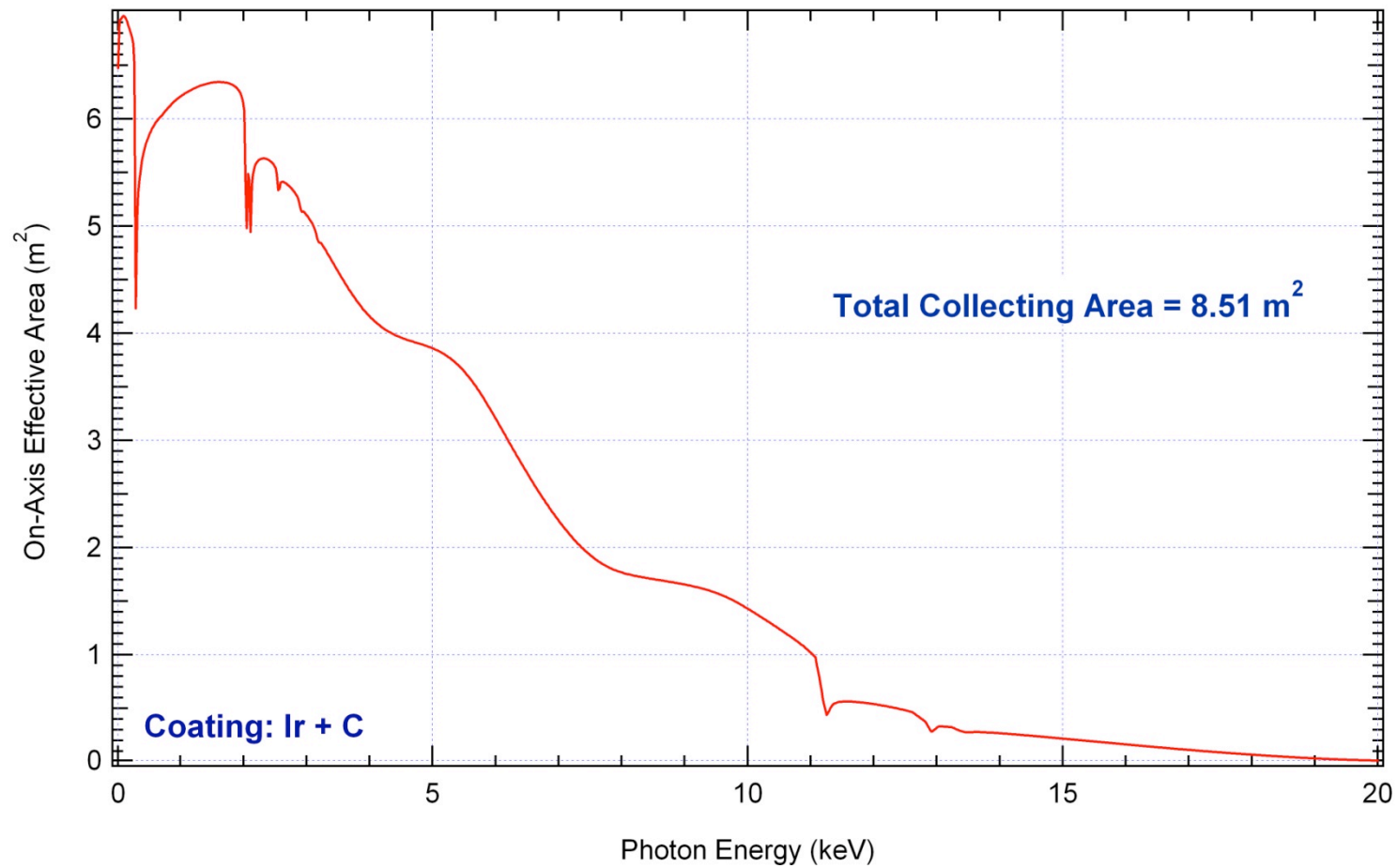
- 3 petal rings, respectively composed by 12 - 24 - 36 petals, arranged on the supporting structure;
- Wolter 1 with focal length 35m; Parabola and hyperbola are 0.6m long (0.3+0.3); 2 mm x 0.15 mm ribs every ~75 mm;
- The total number of mirror shells is 403 made of slumped glass with constant thickness (0.15 mm);

Petal Ring #	Rmin [mm]	Rmax [mm]	Mirror Shells number
1	610	988	192
2	1130	1508	123
3	1660	2027	88

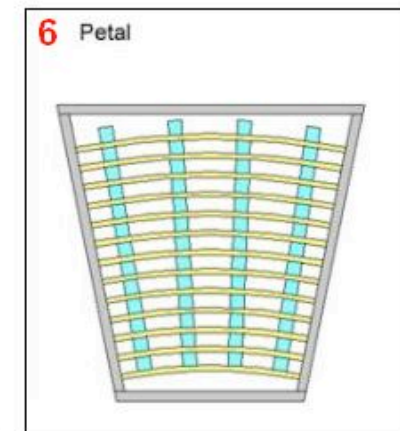
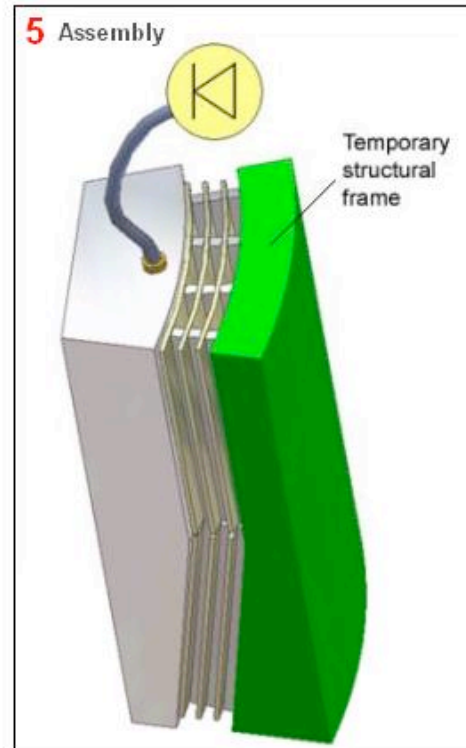
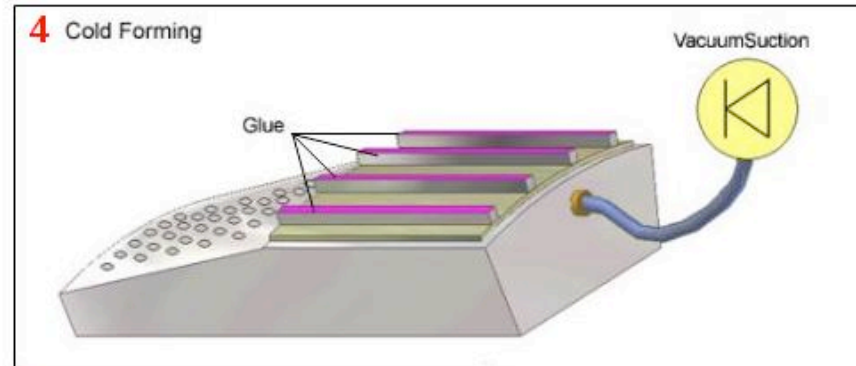
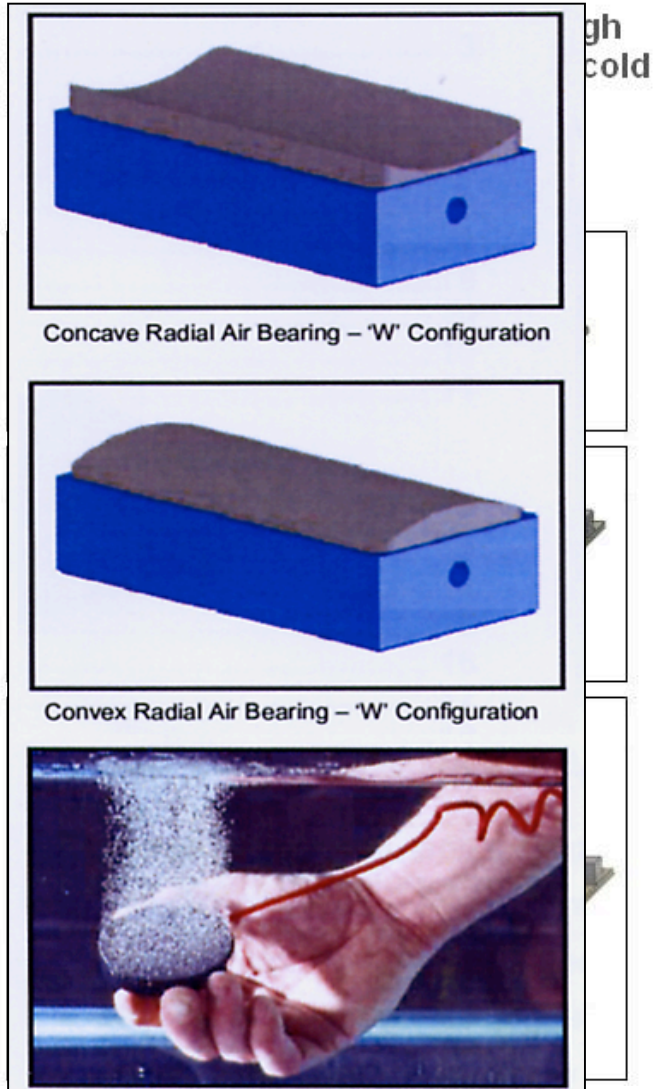


Weight including CFRP Structure ~ 2 tons

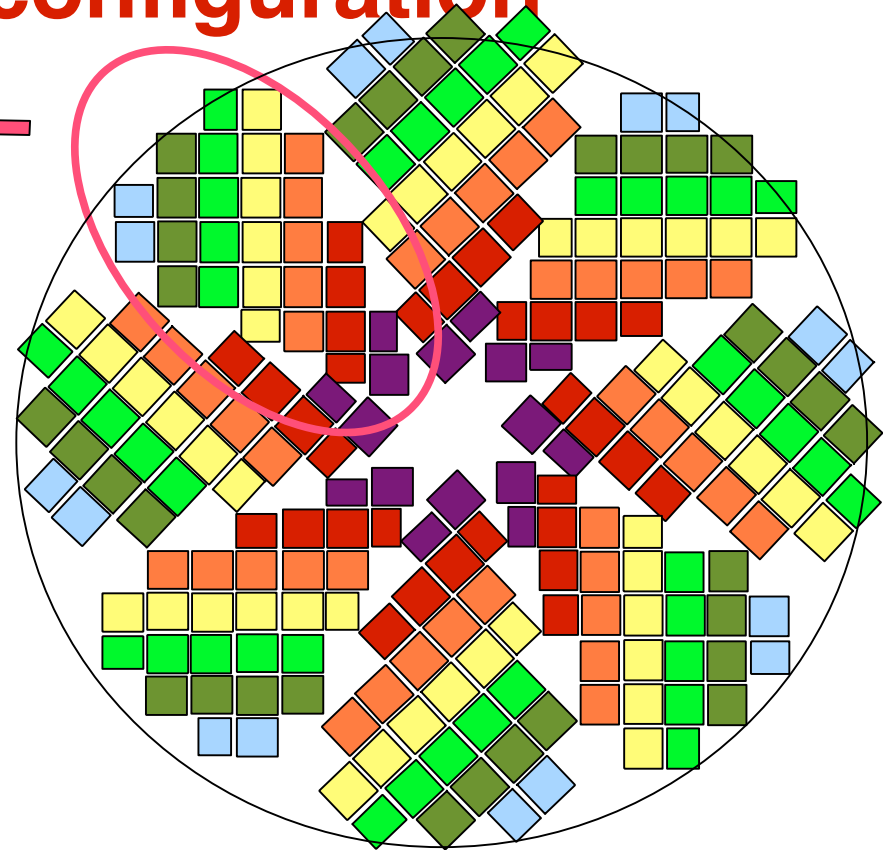
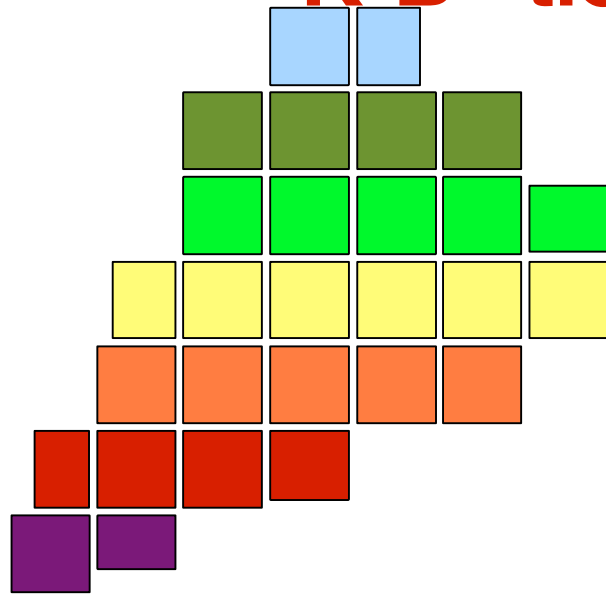
# *Wolter I design effective area*



# Cold slumping glass approach



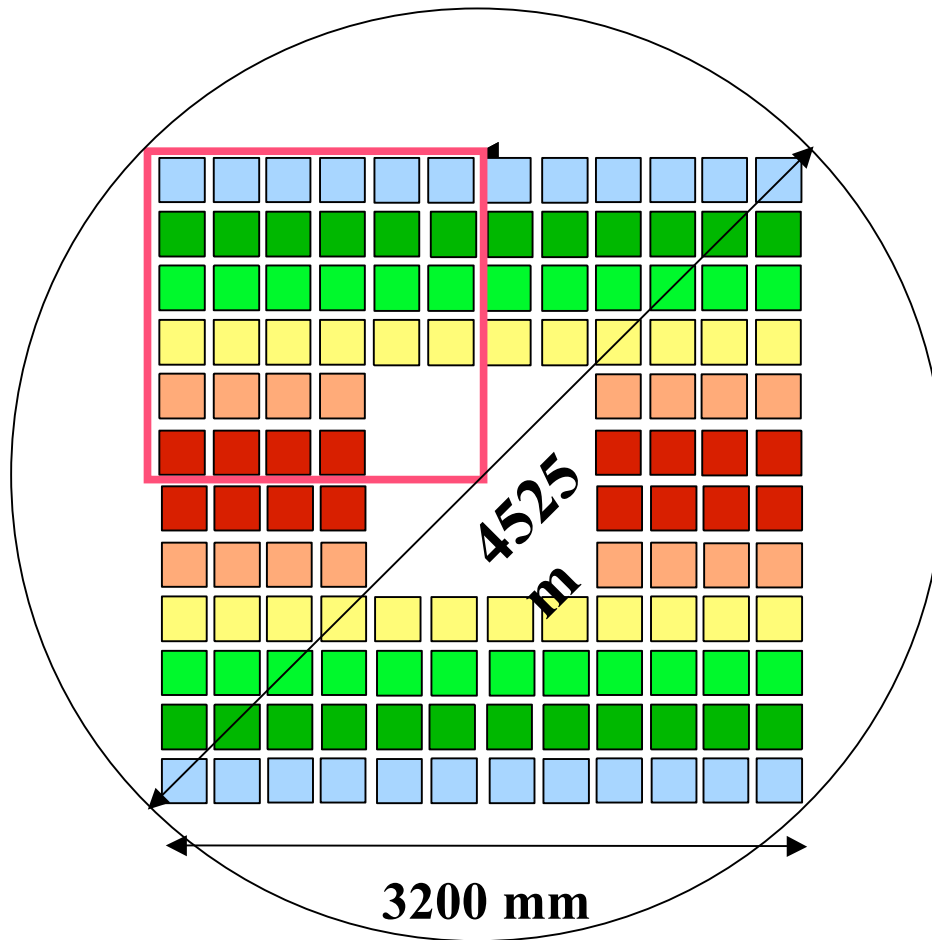
# K-B “tie” type configuration



- Geometry related to fairing dimension
- $L=300 \text{ mm} + 300 \text{ mm}$
- 8 equal petals
- 7 sets of equal blocks for each direction (x, y)\_
- $F=35 \text{ m}$ :  $N1=247$   $N2=243$   $\theta=0.0228 \text{ rad}$
- $F=25 \text{ m}$ :  $N1=180$   $N2=176$   $\theta=0.0365 \text{ rad}$
- $F=20 \text{ m}$ :  $N1=146$   $N2=141$   $\theta=0.0455 \text{ rad}$

4520 mm

# K-B “chocolate” type configuration



- Possibility to use vacant space
- 4 equal modules
- 6 sets of equal blocks for each direction
- $F=35$  m
  - $N1=260$        $N2=258$
  - $\alpha=0,023$  rad
- $F=25$  m
  - $N1=190$      $N2=185$
  - $\alpha=0,032$  rad
- $F=20$  m
  - $N1=151$        $N2=153$
  - $\alpha=0,04$  rad

# LAMAR telescope (1988)\_

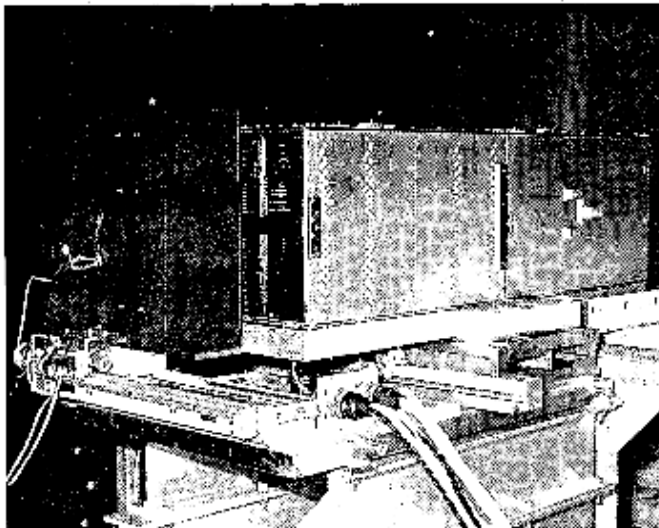


Fig. 2. View of the complete mirror front and rear modules in a vacuum chamber at the MIRC X-Ray Calibration Facility. A 264-cm slit (which is not opened to its full height) defines the direction for the x-ray beam.

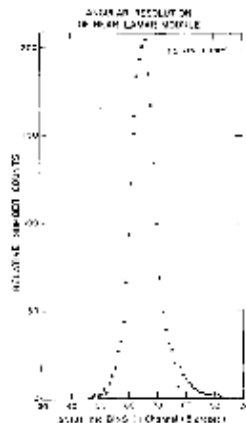


Fig. 3. An early result for the function of the resolution of the mirror at 1.5 keV as measured with the LLU detector. This is the LL image profile along a horizontal axis.

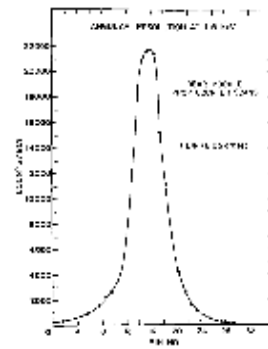


Fig. 4. The 1.5-keV 1-D angular resolution profile at a horizontal axis of the rear section measured with a scanning small aperture proportional counter.

- D. Fabricant, L.M. Cohen, P. Gorenstein

- Mechanical cold shaping technology

- Mirror module 20 X 30 cm

- $F = 3,4$  m

- Effective Area at 1,49 keV  $82,2 \text{ cm}^2$

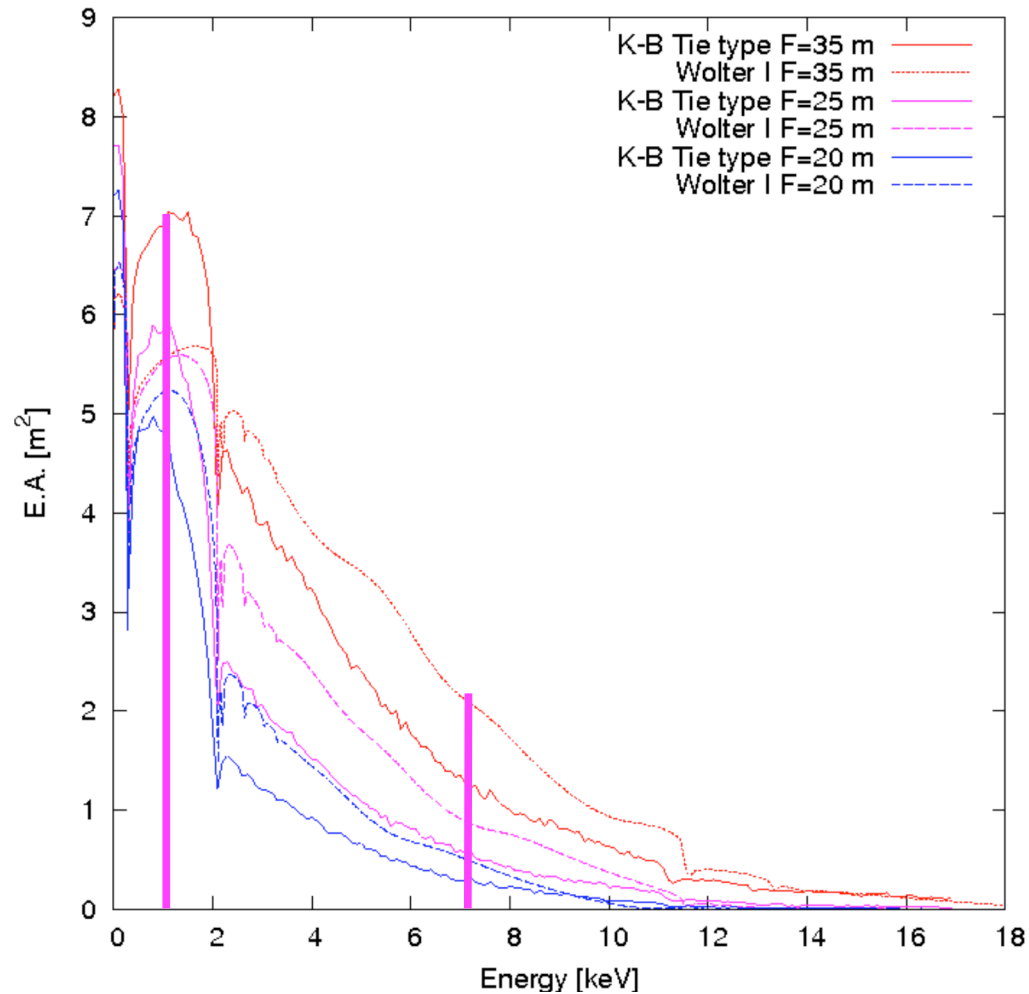
- Effective Area at 8,01 keV  $9,2 \text{ cm}^2$

- HEW 30 arcsec at 1,5 keV



# Effective area

- Effective area: K-B vs Wolter I for different focal length
- Pt+C coating



# Hard X-ray Focusing by mosaic crystals

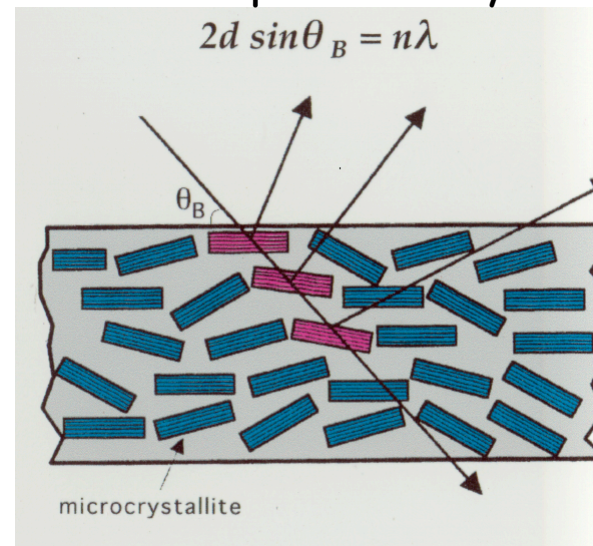
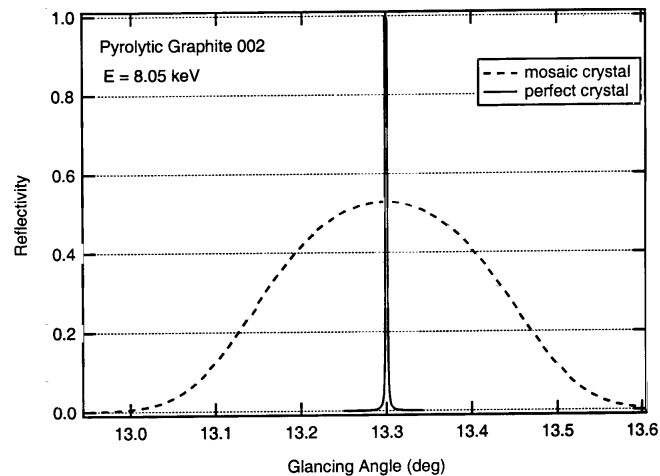
- Bragg diffraction from a crystal lattice  $\rightarrow$  reflectivity peaks at:

$$2 d \sin \theta = n \lambda$$

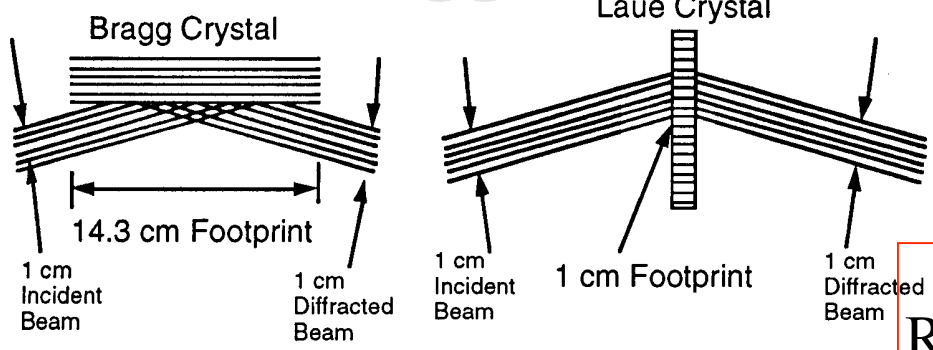
**d** typical value of a few Angstroms

- mosaic crystals: at microscopic level a structure of microcrystals almost-parallel to the external crystal surface. The distribution of the crystallites normals is described by a Gaussian law

- each crystallite reflects in an independent way (without any interferometric coupling with the beams reflected from the other crystallites)  $\rightarrow$  the integrated reflectivity results to be much larger ( $>100$ ) than for a perfect crystal case

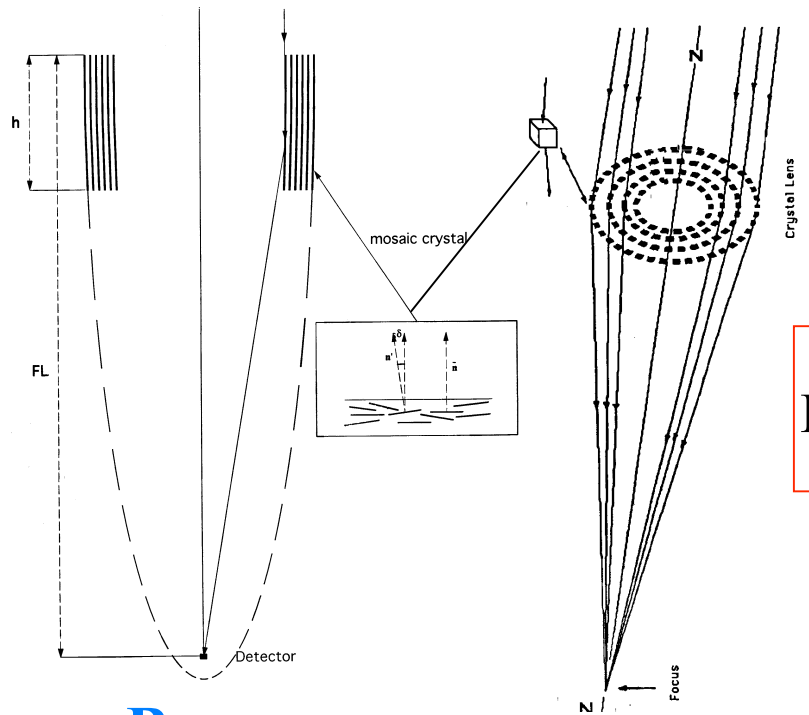


# "Bragg" & "Laue" Configurations



**Bragg**

$$\text{Re } f_{\text{integ}} \propto \left(\frac{F}{V}\right)^2 \lambda^3 \frac{1}{\mu} \times FWHM_{\text{Gauss}}$$



**Laue**

$$\text{Re } f_{\text{integ}} \propto \left(\frac{F}{V}\right)^2 \lambda^3 \frac{T}{\sin \theta} \times FWHM_{\text{Gauss}} \times e^{-\mu \frac{T}{\sin \theta}}$$

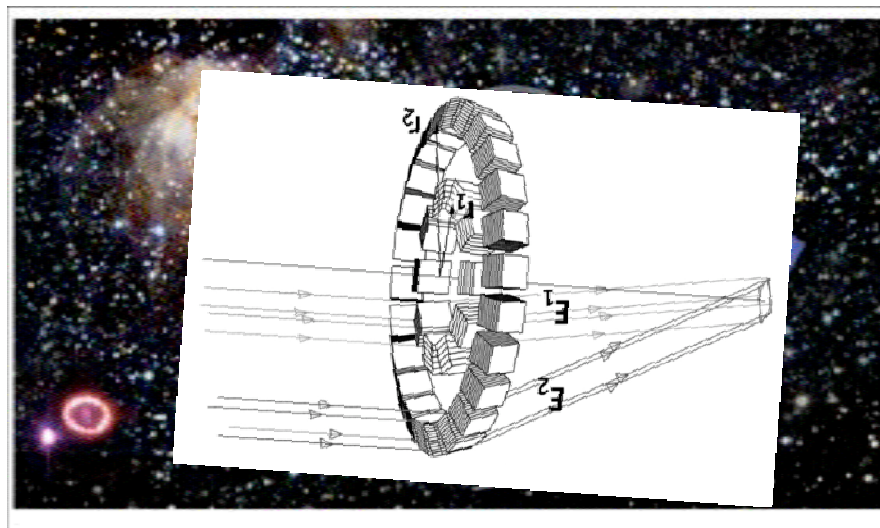
**Bragg**

**Laue**

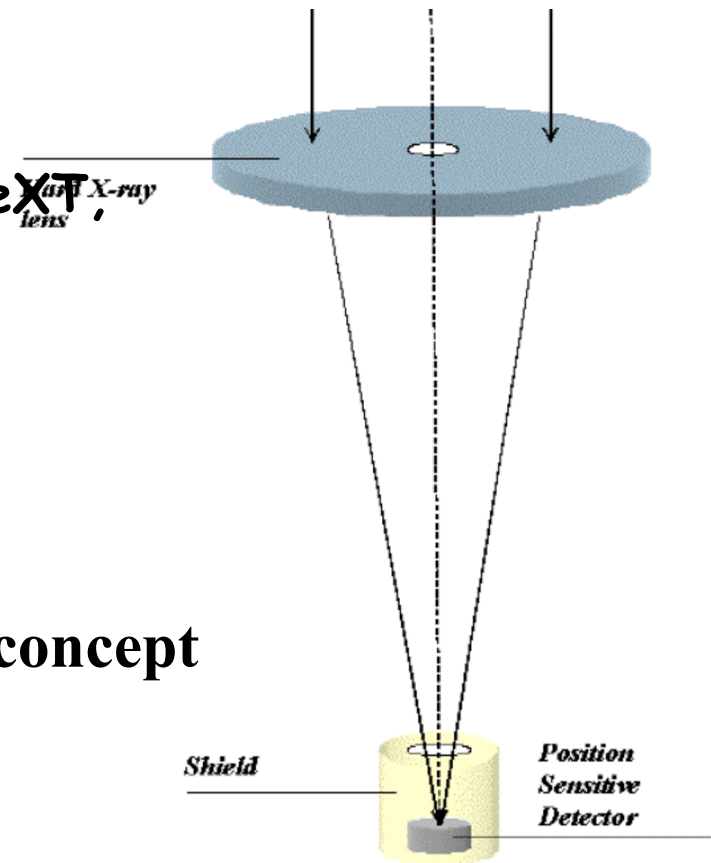
- F = Structure Factor
- V = Volume of the lattice element
- $\mu$  = lin. absorb. coeff

# Why crystal diffraction for high energy telescopes

- Focusing optics in the hard X-/soft gamma-ray band is crucial for a significant leap
- The hard X-ray band ( $E < 80$  keV) can be covered with multilayer mirrors (NuStar, NeXT, Simbol-X).
- The higher energy band ( $> 80$  keV) can be efficiently covered with Laue lenses.

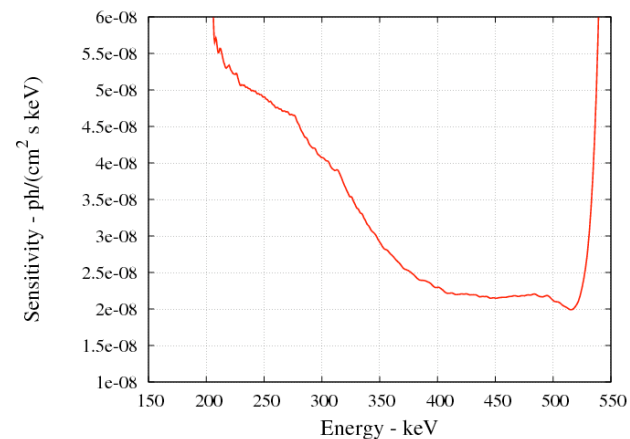
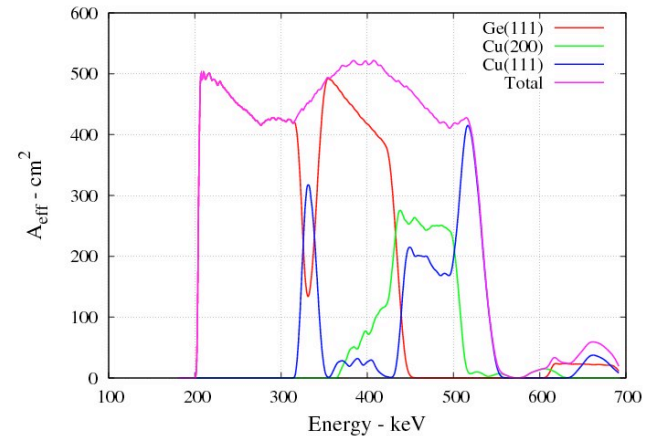


GRI concept



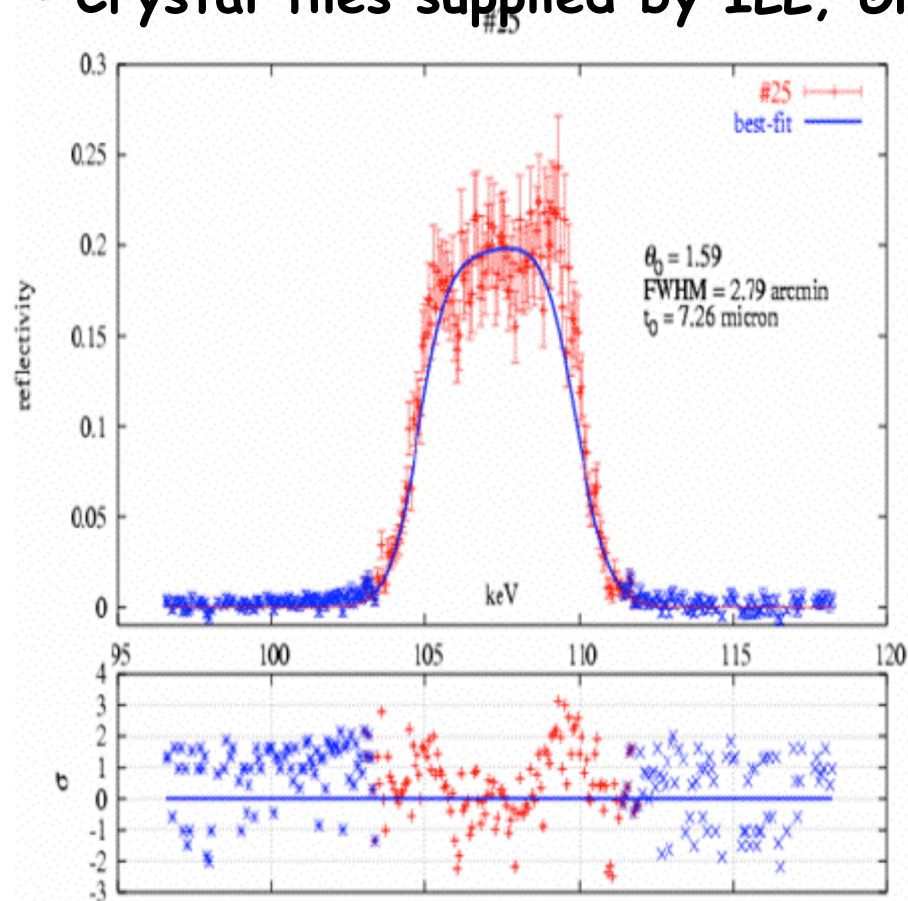
# Example of configuration suitable for GRI low energy lens (200-550 keV)

Parameter	
Focal length (m)	100
Nominal passband (keV)	200-530
Inner radius (cm)	88
Outer radius (cm)	185
Crystal material	Ge[111], Cu[111], Cu[200]
Mosaic spread (arcmin)	0.5
Tile cross section (mm <sup>2</sup> )	15 × 15
Tile thickness (mm)	optimized
Number of crystal rings	61
No. of tiles	17661 (Ge[111]), 3254 (Cu[200]), 3386 (Cu[111])
Crystal weight (kg)	155
Effective area (cm <sup>2</sup> ) @ 200 keV	500
Effective area (cm <sup>2</sup> ) @ 400 keV	530
Effective area (cm <sup>2</sup> ) @ 511 keV	430
Half power radius(mm)	12



**3 sigma sensitivity,  $T = 10^6$  s**

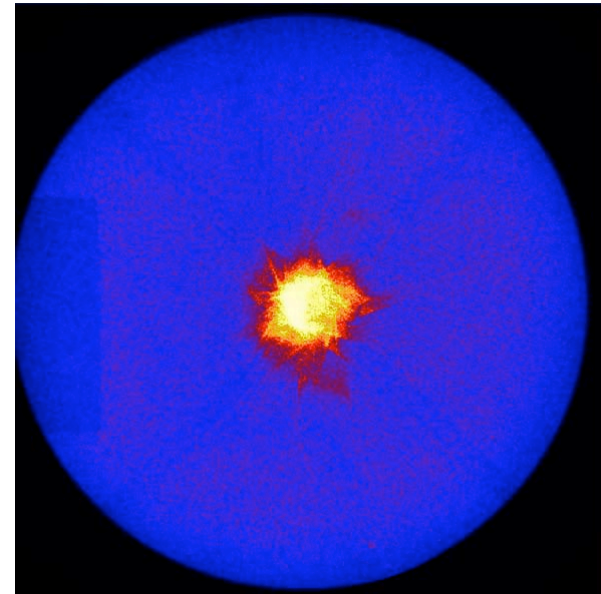
- Crystal material: Cu(111)
- Available mosaic spread: 3-4 arcmin(now also available with lower spread);
- Crystal tiles supplied by ILL, Grenoble.



Credits: F. Frontera – University of Ferrara

# First lens prototype & light

- Tile size: 15x15x2 mm<sup>3</sup>
- Mosaic spread: 3-4 arcmin
- Lens support: carbon fiber
- Focal length: 6 m



**HEW of 15 arcmin at 200 keV**

**Credits;: F. Frontera – University of Ferrara**

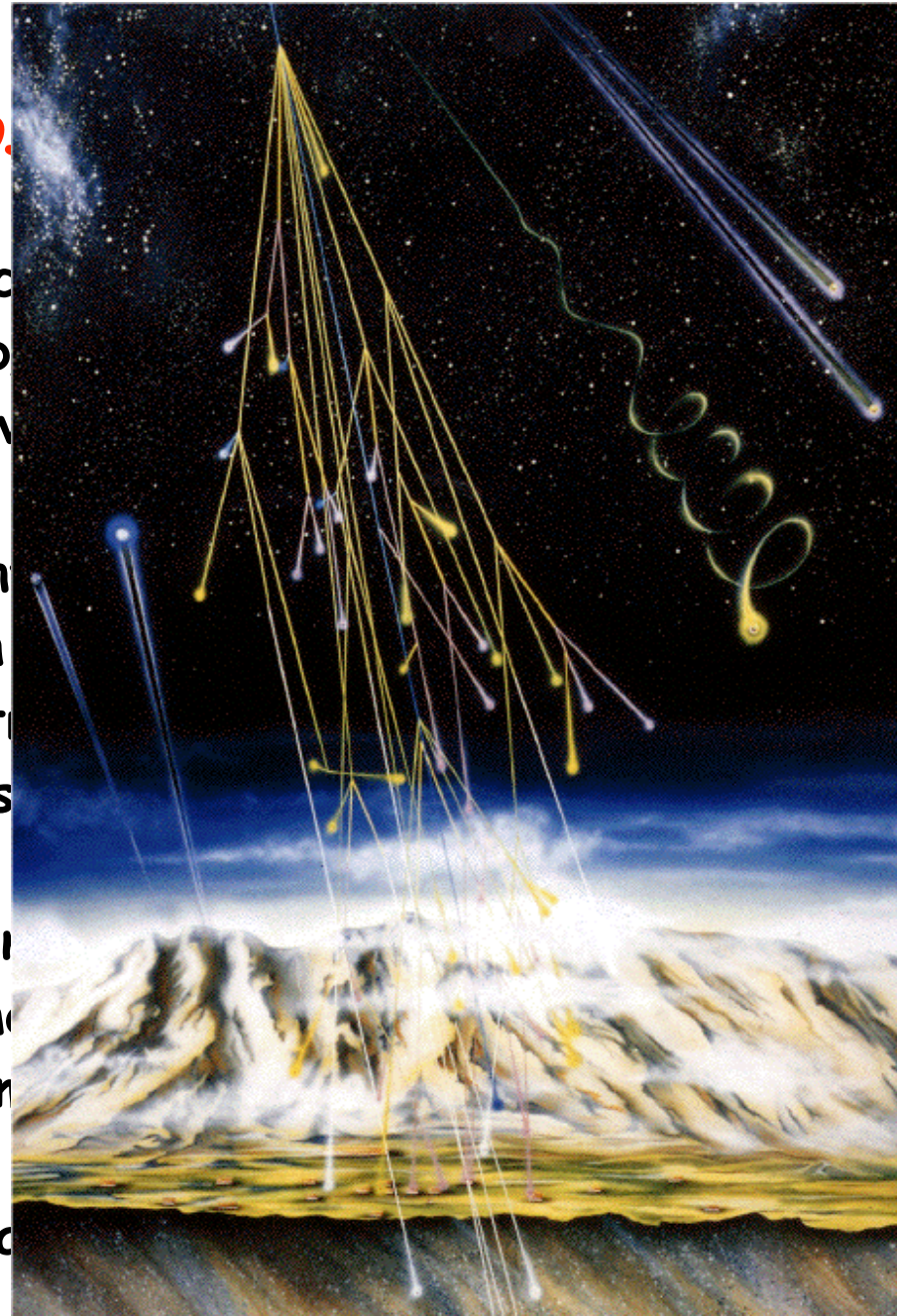
## *Chrenkov Atmospheric Telescopes*

- Atmospheric Cherenkov Telescopes permit to perform observations of astronomical objects emitting in gamma-rays with energies from 50 GeV up to several TeV.
- The showers extend over many kilometers in length and few tens to hundreds of meters in width and have their maximum located at around 8-12 km altitude. Electrons and positrons in the shower core, moves with ultra-relativistic speed and emits Cherenkov light.
- This radiation is mainly concentrated in the near UV and optical band and can therefore pass mostly unattenuated to ground and detected by appropriate instruments.
- Light flashes from showers have a very short duration, typically 2-3 ns in case of a g shower.

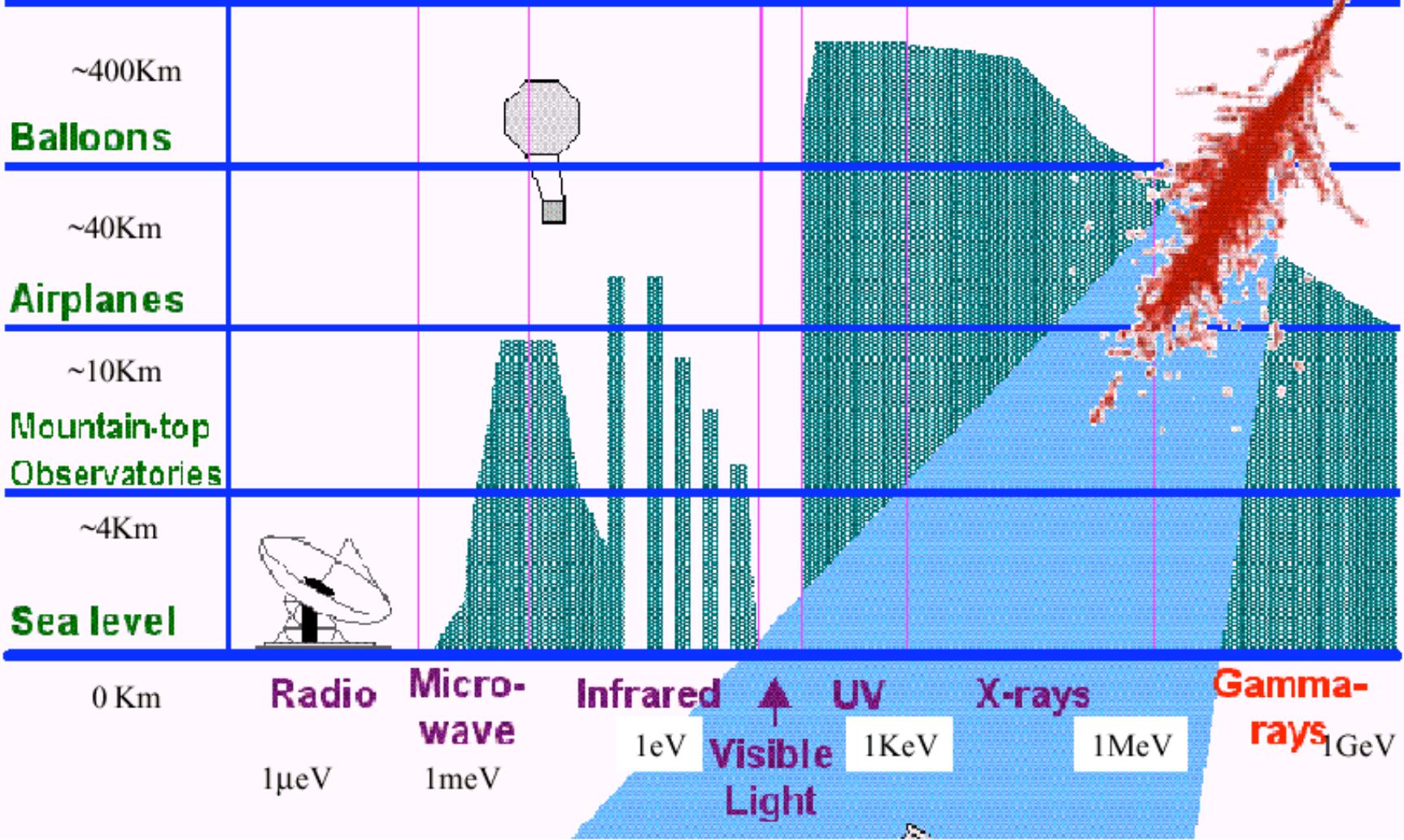


## Cherenkov Atmo.

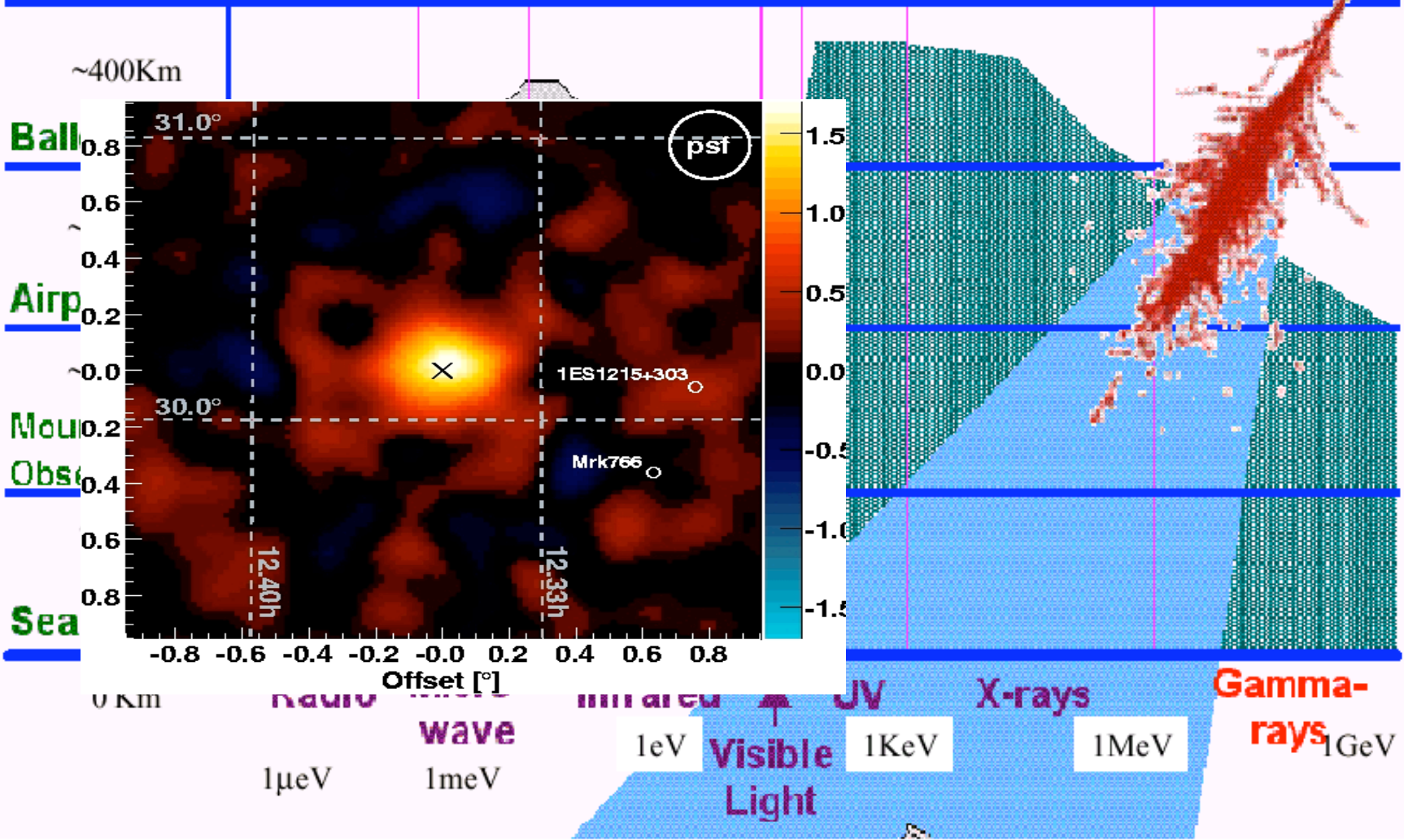
- Atmospheric Cherenkov Telescope observations of astronomical objects at energies from 50 GeV up to several TeV.
- The showers extend over many kilometers to hundreds of meters in width around 8-12 km altitude. Electrons in the core, moving with ultra-relativistic speeds, emit Cherenkov light.
- This radiation is mainly concentrated in the visible and near-ultraviolet band and can therefore pass through the atmosphere to be detected by appropriate instruments.
- Light flashes from showers have a duration of only 2-3 ns in case of a gamma-ray shower.



## Rockets & Satellites



# Rockets & Satellites



## *The MAGIC Telescope Configuration*

- Davies-Cotton reflector, which is the most commonly used configuration for TeV telescopes, is used also for Magic
- Originally, the Davies-Cotton telescope was developed as a solar concentrator and as such, it does not satisfy the rigorous requirements of astronomy in the visible wavelength range
- A large reflector composed of many small, identical, spherical facets is relatively inexpensive to build. The alignment of the optical system is easy.
- A Davies-Cotton telescope consists of a primary mirror with parabolic approximated configuration, formed by several coronas of spherical mirrors each at different radii; the half of central radius coincides with the Focal Length of the primary
- For Magic the focal length is 34 m and the diameter is 17 m; the primary is formed by 240 panels of  $\sim 1 \text{ m}^2$  each

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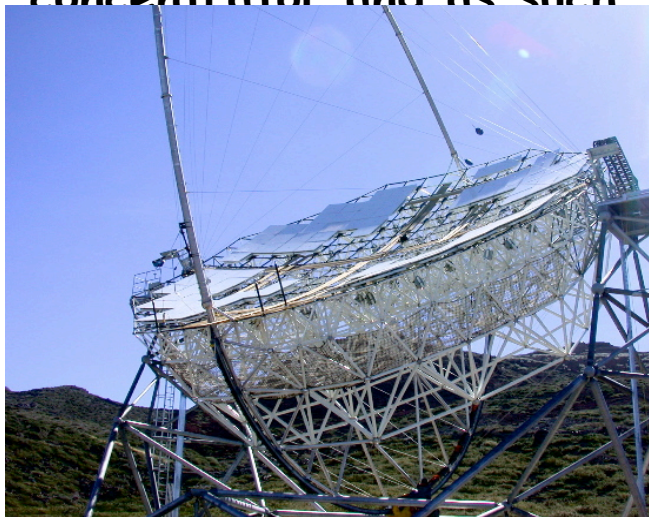
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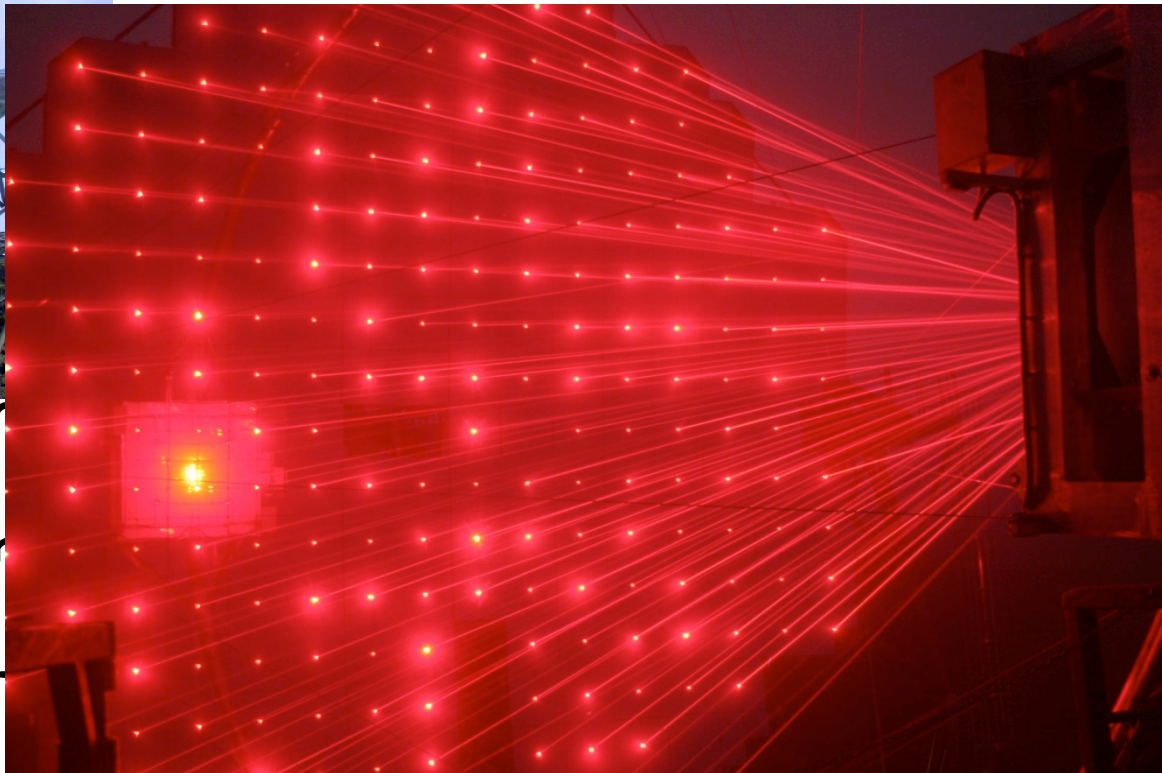
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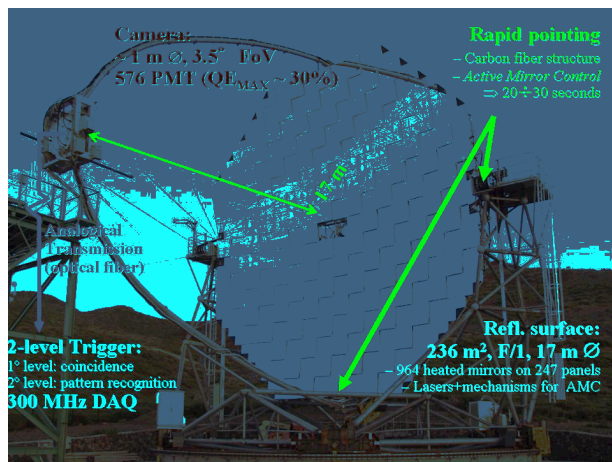
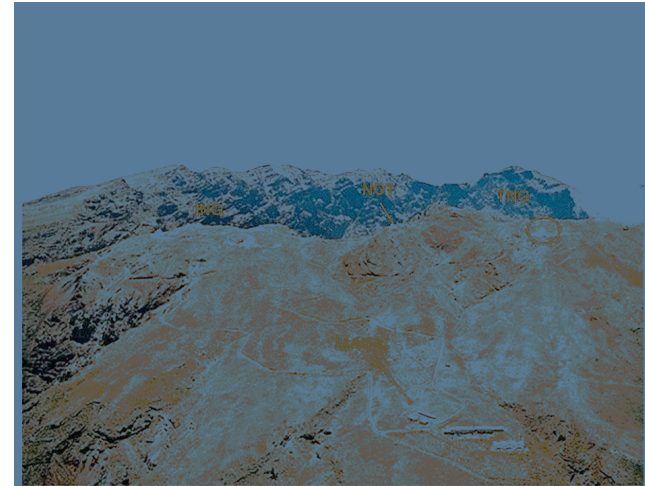
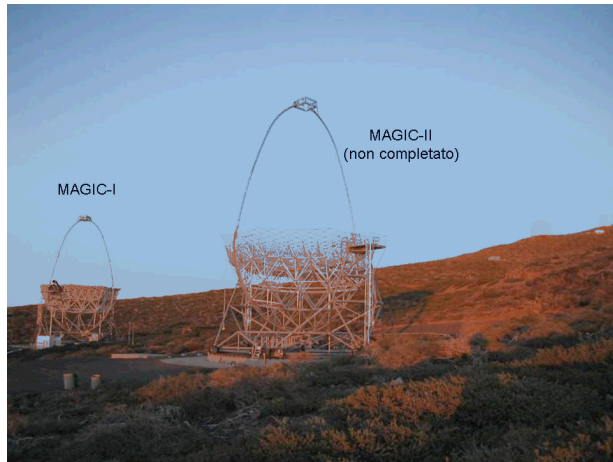


approximated configuration  
mirrors each at different  
the Focal Length of the pr

- For Magic the focal length  
primary is formed by 240



# MAGIC Telescope System



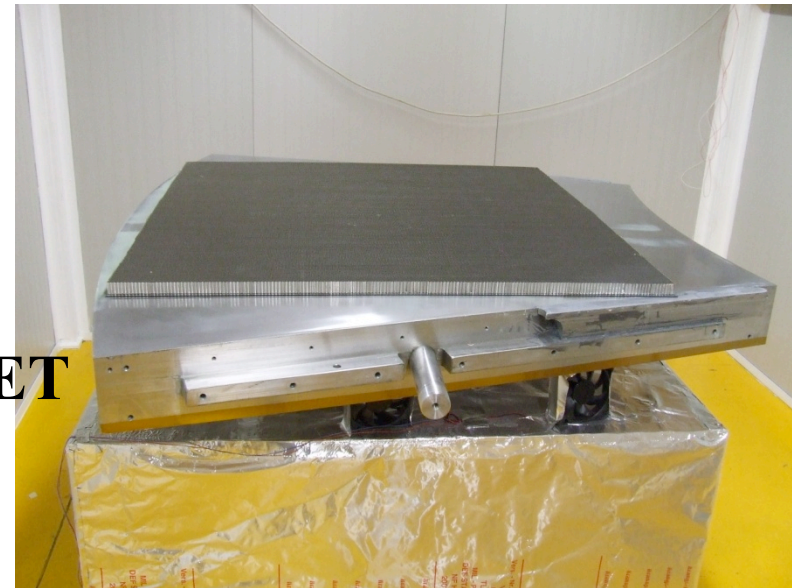
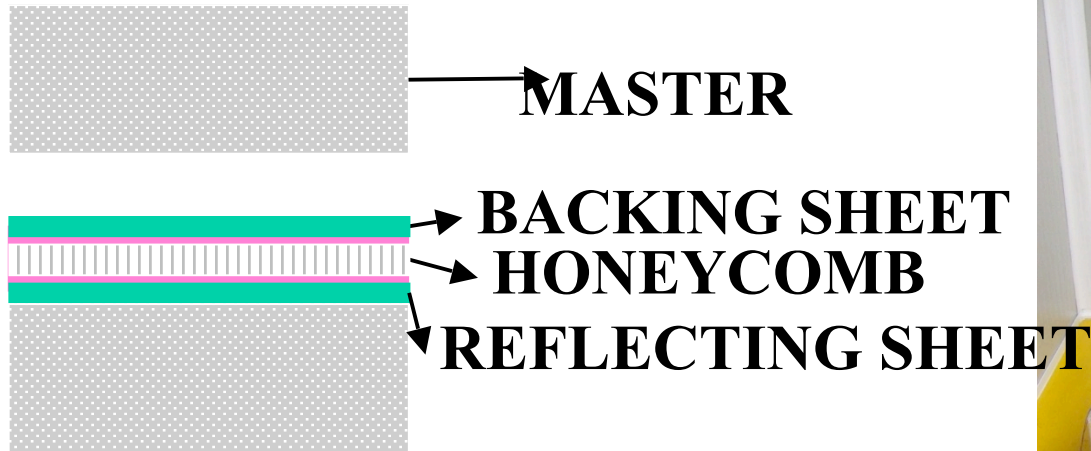
- **Geometry:** Parabolic
- **Diameter:** 17m
- **Collecting Area:** 240 m<sup>2</sup>
- **F-number (f/D):** 1
- **FOV:** 3.8 deg
- **Slew time:** 20 s
- **Angular resolution:** < 3 arcmin
- **Energy Resolution:** 30%
- **Operating Band:** 50 GeV – 50 TeV
- **Sensitivity (@1 TeV):** 30 mCrab (1 single telescope)  
20mCrab (2 telescopes)
- **Sensitivity @ 50 GeV:** 0.1 Crab (1 single telescope)  
0.05 Crab (2 telescopes)

# *Glass Mirror Manufacturing*

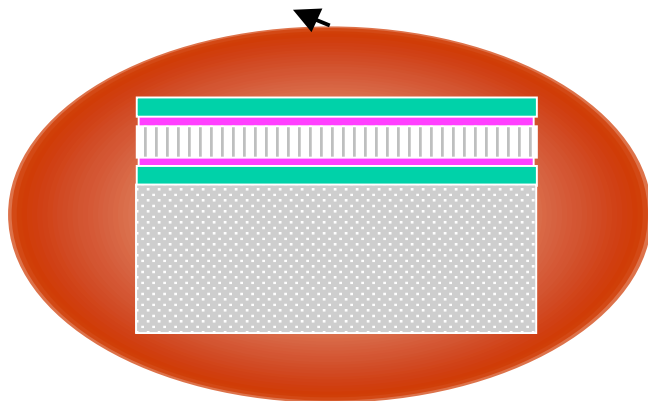
- Derived from a similar technique proposed by for the manufacturing of X-Ray optics (XEUS)
- A thin glass sheet (1-2 mm) is elastically deformed so as to retain the shape imparted by a master with convex profile. If the radius of curvature is large, the sheet can be pressed against the master using vacuum suction
- On the deformed glass sheet (under vacuum force) one glues a honeycomb structure that provides the needed rigidity
- Then a second glass sheet is glued on the top in order to obtain a sandwich
- After releasing the vacuum, on the concave side one deposits a reflecting coating (Aluminum) and a thin protective coating (Quartz)



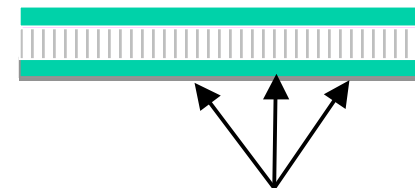
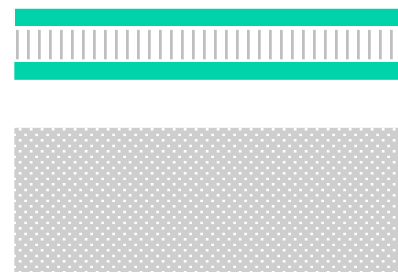
# *Glass Panel Manufacturing flow*



**CURING CHAMBER**



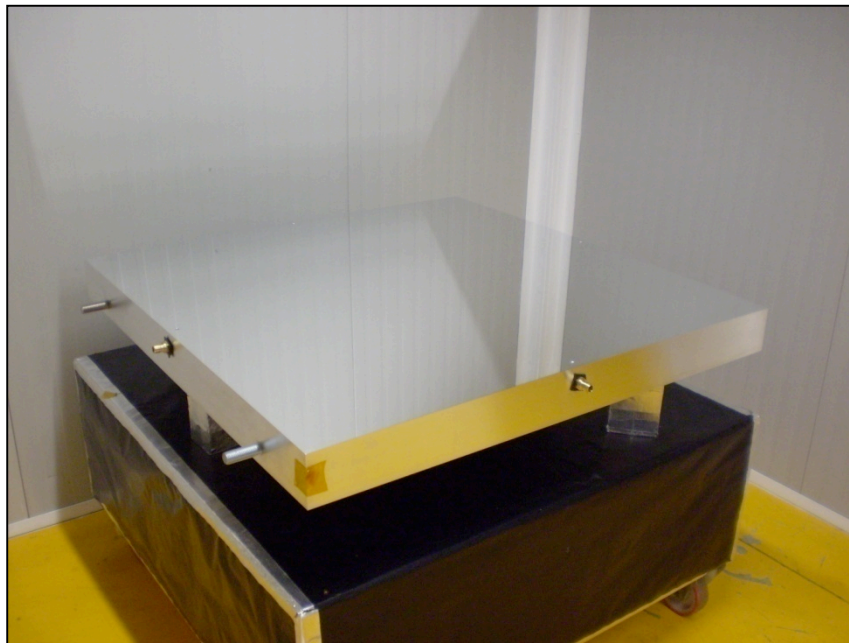
**RELEASE**



**PVD COATING**

**AL + SiO<sub>2</sub>**

## *Master and panel in the making*



**Aluminum master 1040 x  
1040 mm**

**Front and rear of a segment  
Size = 985 x 985 mm Weight = 9.5 Kg.  
Nominal curvature radius= 35 m**



MAGIC CT2 Fri Jul 25 13:50:01 2008



All 240 panels successfully produced, being installed right now!